Proposed Subdivision
Billy's Lookout - Stage 7
Site Classification

Fishermans Drive, Teralba

NEW15P-0070A-AK 27 March 2018



27 March 2018

McCloy Development Management Pty Ltd Suite 1, Level 3, 426 King Street NEWCASTLE WEST NSW 2309

Attention: Jon Hines

Dear Sir.

RE: PROPOSED SUBDIVISION – BILLY'S LOOKOUT – STAGE 7
FISHERMANS DRIVE, TERALBA
SITE CLASSIFICATION (LOTS 701 TO 730)

Please find enclosed our geotechnical report for Stage 7 of the residential subdivision of Billy's Lookout, located at Fishermans Drive, Teralba.

The report provides site classification with respect to reactive soils, in accordance with the requirements of AS2870-2011 'Residential Slabs and Footings', Stage 7 (Lots 701 to 730).

If you have any questions regarding this report, please do not hesitate to contact Shannon Kelly or the undersigned.

For and on behalf of Qualtest Laboratory (NSW) Pty Ltd

Jason Lee

Principal Geotechnical Engineer

Table of Contents:

1.0		Introduction	1
2.0		Desktop Study	
3.0		Field Work	1
4.0		Site Description	2
	4.1	Site Regrade Works	. 2
	4.2	Surface Conditions	. 2
	4.3	Subsurface Conditions	.:
5.0		Laboratory Testing	7
6.0		Site Classification to AS2870-2011	8
7.0		Limitations	c

Attachments:

Figure AK1: Approximate Test Location Plan

Appendix A: Engineering Logs of Test Pits

Appendix B: Results of Laboratory Testing

Appendix C: CSIRO Sheet BTF 18 - Foundation Maintenance and Footing Performance

NEW15P-0070A-AK

1.0 Introduction

Qualtest Laboratory NSW Pty Ltd (Qualtest) is pleased to present this site classification report on behalf of McCloy Development Management Pty Ltd (McCloy), for Stage 7 of the residential subdivision of Billy's Lookout, located at Fishermans Drive, Teralba.

Based on the brief and drawing provided by the client, Stage 7 is understood to comprise of 30 residential allotments (Lots 701 to 730).

The scope of work for the geotechnical investigation included providing site classification with respect to reactive soils, in accordance with the requirements of AS2870-2011 'Residential Slabs and Footings', for Stage 7 following completion of site regrade works.

This report presents the results of the field work investigations and laboratory testing, and provides recommendations for the scope outlined above.

2.0 Desktop Study

The scope of work has included a review of the following reports completed by Qualtest:

- Site Classification report, 'Proposed Subdivision, Billy's Lookout Stage 7, Fishermans Drive, Teralba, (Report Reference: NEW15P-0070A-AI, dated 6 September 2017);
- Site Classification report, 'Proposed Subdivision, Billy's Lookout Stages 5 to 9, Fishermans Drive, Teralba, (Report Reference: NEW15P-0070A-AA, dated 16 February 2016);
- Site Classification report, 'Proposed Subdivision, Billy's Lookout Stage 5, Fishermans Drive, Teralba, (Report Reference: NEW15P-0070A-AB, dated 16 June 2016);
- Site Classification report, 'Proposed Subdivision, Billy's Lookout Stage 5, Fishermans Drive, Teralba, (Report Reference: NEW15P-0070A-AH, dated 11 August 2017);
- Site Classification report, 'Proposed Subdivision, Billy's Lookout Stages 6 & 9, Fishermans Drive, Teralba, (Report Reference: NEW15P-0070A-AJ, dated 15 November 2017);

This report includes a summary of selected results from the previous reports where applicable.

3.0 Field Work

Following site regrade works, additional field work investigations were carried out on 6 March 2018, comprising of:

- Excavation of fourteen test pits (TP701 to TP714) using a 5 tonne tracked excavator with a 0.30m wide toothed bucket, to depths of between 0.21m – 2.00m;
- Small disturbed samples were taken for subsequent laboratory testing;
- Test pits were backfilled with the excavation spoil and compacted using the excavator bucket and tracks.

Investigations were carried out by an experienced Geotechnical Engineer from Qualtest who located the test pits, carried out the testing and sampling, produced field logs of the test pits, and made observations of the site surface conditions.

Approximate test pit locations are shown on the attached Figure AK1, which also includes test pit locations from the previous investigations conducted on site. Engineering logs of the test pits are presented in Appendix A. Density estimates for granular materials shown on the logs were assessed based upon visual and tactile observations only.

4.0 **Site Description**

4.1 **Site Regrade Works**

Site re-grading works were conducted on Lots 701 to 730 within Stage 7. It is understood that for the majority of lots, site re-grade works were limited to cutting to varying depths, and typically placement of fill (mostly topsoil) to depths of less than or equal to 0.4m.

Lots 702, 703, 706 and 707 have been filled using approved site won material. Prior to filling, lot re-grade areas were stripped of all topsoil and unsuitable material to expose suitable natural residual foundation profile. Re-grade works then consisted of filling with approved site fill to finish design levels.

Filling was performed using site material won from excavations cut from around the site. The fill material could generally be described as mixtures of Sandy Gravelly CLAY, and Sandy CLAY, of medium plasticity, with fine to coarse grained sand and gravel (from weathered rock).

As the geotechnical testing authority engaged for the project, we state that the filling performed for the regrade areas (Lots 702, 703, 706 and 707), was carried out to Level 1 criteria as defined in Clause 8.2 - Section 8, of AS3798-2007, 'Guidelines on Earthworks for Commercial and Residential Developments'.

Reference should be made to 'Level 1 Site Re-grade Assessment Report' (Qualtest Ref: NEW17P-0199-AA) for details of the site regrade works conducted by Qualtest.

The recommendations of this report are based on the understanding that any existing lot re-grade works outside the areas described above are limited to cutting and/or placement of fill such that total fill and topsoil depths do not exceed 0.4m. Qualtest should be informed without delay if additional earthworks are known to have been carried out.

4.2 **Surface Conditions**

Selected photographs of the site are shown below.



corner of Lot 705, Excavator at TP702.



Photograph 1: Facing south from near northern **Photograph 2:** Facing southwest from near northern corner of Lot 705.



Photograph 3: Facing east from near TP706, Wheelhouse Road visible in background.



Photograph 4: Facing southeast from near TP706 (from Lot 729).



Photograph 5: Facing east from Lot 706.



Photograph 6: Facing southeast from Lot 706.

4.3 Subsurface Conditions

Reference to the 1:100,000 Newcastle Coalfield Regional Geology Sheet indicates the site to be underlain by the Clifton Subgroup of the Narrabeen Group, and the Moon Island Beach Subgroup of the Newcastle Coal Measures, which are characterised by Conglomerate, Sandstone, Siltstone, Claystone, Tuff and Coal rock types.

Table 1 presents a summary of the typical soil types encountered on site during the field investigations, divided into representative geotechnical units.

Table 2 contains a summary of the distribution of the above geotechnical units at the test pit locations.

No groundwater levels or water inflows were encountered in the test pits during the limited time that they remained open on the day of the field investigation.

It should be noted that groundwater conditions can vary due to rainfall and other influences including regional groundwater flow, temperature, permeability, recharge areas, surface condition, and subsoil drainage.

Reference should be made to the previous reports outlined in Section 2.0 for further details of site description, subsurface conditions, field work conducted, engineering logs of test pits, laboratory testing results, site supervision and density testing carried out as part of those previous assessments.

TABLE 1 – SUMMARY OF GEOTECHNICAL UNITS AND SOIL TYPES

Unit	Soil Type	Description
1A	FILL – TOPSOIL & MULCH	Generally up to about 50mm of mulch, overlying Sandy CLAY / Clayey SAND – low to medium plasticity, fine to coarse grained, dark grey to grey, low to medium plasticity, with some fine to medium grained gravel in places, root affected in places.
1B	FILL	Sandy CLAY – medium and low to medium plasticity, dark grey-brown, orange-brown to dark orange and pale grey-white, fine to coarse grained sand, with some fine to medium grained sub-angular to sub-rounded gravel and trace cobbles in places. SAND – fine to coarse grained, grey. Clayey SAND – fine to coarse grained, grey to grey-brown, fines of low to medium plasticity, trace fine to medium grained sub-rounded to sub-angular gravel.
2	TOPSOIL	Silty SAND - fine to coarse grained, grey, fines of low plasticity, root affected. Clayey SAND - fine to coarse grained, dark brown to grey, fines of medium plasticity, root affected.
3	SLOPEWASH / COLLUVIUM	Silty SAND, SAND - fine to medium grained, pale brown / grey, some Silt / fines of low plasticity. Clayey SAND - fine to coarse grained, dark brown to grey, fines of medium plasticity.
4	residual soil	Silty CLAY / Sandy CLAY – medium and medium to high plasticity, variable colours such as pale brown, orange to pale brown, pale grey, grey, and brown to red, some sand / fine to coarse grained sand. Clayey SAND / SAND – fine to coarse grained, orange-brown and pale grey-white, with clay / fines of low to medium plasticity, trace fine to medium grained sub-angular to sub-rounded gravel.
5	EXTREMELY WEATHERED (XW) ROCK	Extremely Weathered Sandy SILTSTONE / SANDSTONE with Soil Properties; excavating as SAND – fine to coarse grained, pale greywhite and orange-brown to orange, with some clay. Breaks down into Clayey SAND in places.
6	HIGHLY WEATHERED (HW) ROCK	SANDSTONE - fine to coarse grained, variable colours such as pale grey to white, grey, orange, pale brown, variable estimated strength ranging from low to high. Sandy SILTSTONE – pale orange-brown to brown and pale grey, estimated medium strength, with some Extremely Weathered pockets.

TABLE 2 – SUMMARY OF GEOTECHNICAL UNITS ENCOUNTERED AT TEST PIT LOCATIONS

TEST PIT NO.	UNIT 1A Fill – Mulch & Topsoil	UNIT 1B Fill	UNIT 2 Topsoil	Unit 3 Slopewash / Colluvium	Unit 4 Residual Soil	Unit 5 XW Rock	Unit 6 HW Rock
				Depth (m)			
		Current Geotech	ınical Assessment (Ref: NEW15P-0070A	-AK, March 2018)		
TP701	0.00 - 0.25	-	-	-	0.25 - 2.00	-	-
TP702	0.00 - 0.25	-	-	0.25 - 0.40	0.40 - 0.70	-	0.70 - 0.71*
TP703	0.00 - 0.20	0.20 - 0.40	-	-	-	-	0.40 - 0.41*
TP704	0.00 - 0.18	-	-	-	0.18 - 0.80	-	0.80 - 0.81*
TP705	0.00 - 0.20	-	-	-	-	-	0.20 - 0.21*
TP706	0.00 - 0.25	-	-	-	0.25 - 0.60	-	0.60 - 0.61*
TP707	0.00 - 0.35	-	-	-	-	0.35 - 0.75	0.75 - 0.77*
TP708	0.00 - 0.20	-	-	-	0.20 - 0.25	0.25 - 0.65	0.65 - 0.66*
TP709	0.00 - 0.20	-	-	-	-	0.20 - 0.30	0.30 - 0.33*
TP710	-	-	-	-	-	0.00 - 0.25	0.25 - 0.28*
TP711	0.00 - 0.38	-	-	-	-	0.38 - 1.30	1.30 - 1.35*
TP712	0.00 - 0.06	0.06 - 0.25	-	-	0.25 - 1.00	-	1.00 - 1.15*
TP713	0.00 - 0.25	-	-	-	-	-	0.25 - 0.30*
TP714	0.00 - 0.25	-	-	-	-	0.25 - 1.40^	-
	F	Previous Geotechn	ical Assessment (R	ef: NEW15P-0070A-	AJ, November 2017)	
TP601	-	-	0.00 - 0.25	-	-	-	0.25 - 0.35*
TP602	0.00 - 0.20	-	-	-	0.20 - 0.25	-	0.25 - 0.27*

TEST PIT NO.	UNIT 1A Fill – Mulch & Topsoil	UNIT 1B Fill	UNIT 2 Topsoil	Unit 3 Slopewash / Colluvium	Unit 4 Residual Soil	Unit 5 XW Rock	Unit 6 HW Rock
				Depth (m)			
TP903	0.00 - 0.20	-	-	-	-	-	0.20 - 0.25*
	•	Previous Geotech	nical Assessment (Ref: NEW15P-0070A	-AH, August 2017)		•
TP5-3	0.00 - 0.20	0.20 - 0.95	-	-	0.95 - 1.50	-	-
TP5-5	0.00 - 0.25	0.25 - 1.20	-	-	1.20 - 1.40	-	-
		Previous Geotec	hnical Assessment	(Ref: NEW15P-0070	A-AB, June 2016)		
TP204	-	-	0.00 - 0.18	0.18 - 0.27	0.27 - 0.40	-	0.40 - 0.65#
		Previous Geotechn	ical Assessment (R	Ref: NEW15P-0070A-	AA, February 2016)		
TP105	-	-	0.00 - 0.25	-	0.25 - 1.00	-	1.00 - 2.30^
TP107	-	-	0.00 - 0.20	-	0.20 - 0.50	-	0.50 - 0.75*
TP108	-	-	0.00 - 0.20	-	0.20 - 0.70	-	0.70 - 0.80*
TP111	-	-	0.00 - 0.15	-	0.15 - 0.45	-	0.45 - 0.50*
TP112	-	-	0.00 - 0.25	-	0.25 - 0.80	-	0.80 - 0.90*
Notes:	* = Practical refus	sal or refusal of 5 to	nne excavator me	t on Highly Weathe	red Rock.		

^{# =} Practical refusal or refusal of 22 tonne excavator met on Highly Weathered Rock (preliminary investigation Feb 2016).

 $[\]wedge$ = Slow to very slow progress, close to practical excavator refusal.

5.0 Laboratory Testing

Samples collected during the field investigations were returned to our NATA accredited Warabrook Laboratory for testing which comprised of:

• (12 no.) Atterberg Limits tests.

Results of the laboratory testing are presented in Appendix B, with a summary of the Atterberg Limits test results presented in Table 3.

Table 3 and Table 4 also include a summary of laboratory testing information (where applicable) from the previous Geotechnical Assessment works carried out by Qualtest.

TABLE 3 – SUMMARY OF ATTERBERG LIMITS TESTING RESULTS

Location	Depth (m)	Material Description	Liquid Limit (%)	Plastic Limit (%)	Plasticity Index (%)	Linear Shrinkage (%)
		Current Investigation	(March 20)18)		
TP701	0.80 – 1.00	(CH) Silty CLAY	52	17	35	9.0
TP702	0.40 - 0.60	(SC) Clayey SAND	39	18	21	7.0
TP703	0.05 – 0.20	FILL: TOPSOIL (CL) Sandy CLAY	24	16	8	3.5
TP704	0.20 - 0.40	(SC) Gravelly Clayey SAND	26	17	9	4.0
TP705	0.10 - 0.20	FILL: TOPSOIL (CL) Sandy CLAY	24	18	6	3.0
TP706	0.30 - 0.50	(SC) Clayey SAND	27	17	10	3.5
TP707	0.60 – 0.70	(EW) Extremely Weathered Sandstone with soil properties	30	15	15	5.0
TP708	0.30 - 0.50	(EW) Extremely Weathered Sandstone with soil properties	26	16	10	4.0
TP711	0.10 - 0.20	FILL: TOPSOIL (SC) Clayey SAND	26	19	7	3.0
TP711	0.40 – 0.60	(EW) Extremely Weathered Sandstone with soil properties	36	16	20	7.0
TP712	0.30 – 0.50	(CH) Sandy CLAY	52	21	31	9.0

Location	Depth (m)	Material Description	Liquid Limit (%)	Plastic Limit (%)	Plasticity Index (%)	Linear Shrinkage (%)		
TP714	0.30 - 0.50	(EW) Extremely Weathered Sandy Siltstone with soil properties	43	20	23	7.0		
	Previ	ous Investigation (June 2016 & November 2017)						
TP204	0.30 - 0.40	(CH) Sandy CLAY	68	19	49	16.0		
TP602	0.20 – 0.25	(SC) Clayey SAND	27	17	10	3.5		
TP903	0.10 - 0.20	FILL: (SC) Clayey	23	15	8	3.0		

Table 4 presents a summary of shrink/swell test results from the previous Geotechnical Assessment works carried out by Qualtest.

TABLE 4 - SUMMARY OF SHRINK / SWELL TESTING RESULTS

Location	Depth (m)	Material Description	I _{ss} (%)
	Previous In	vestigations (February 2016 & August 2017)	
TP5-5	0.40 - 0.80	FILL: (CH) Sandy CLAY	0.9
TP105	0.40 - 0.80	(CH) CLAY	1.3
TP112	0.30 – 0.55	(CH) Sandy CLAY	1.1

6.0 Site Classification to AS2870-2011

Based on the results of the field work, laboratory testing, and Level 1 site supervision and testing carried out, residential lots located within Stage 7 of the Billy's Lookout subdivision located Fishermans Drive, Teralba, as shown on Figure AK1, are classified in their current condition in accordance with AS2870-2011 'Residential Slabs and Footings', as shown in Table 5.

TABLE 5 - SITE CLASSIFICATION TO AS2870-2011

Stage	Lot Numbers	Site Classification	Estimated Characteristic Free Surface Movement
7	Lots 701 to 730	M	20mm to 40mm

Characteristic free surface movements have been estimated for lots in their existing condition as shown in Table 5.

The effects of changes to the soil profile by additional cutting and filling and the effects of past and future trees should be considered in selection of the design value for differential movement.

If site re-grading works involving cutting or filling are performed after the date of this assessment the classification may change and further advice should be sought.

Final site classification will be dependent on the type of fill and level of supervision carried out. Re-classification of lots should be confirmed by the geotechnical authority at the time of construction following any site re-grade works.

Footings for the proposed development should be designed and constructed in accordance with the requirements of AS2870-2011.

The classification presented above assumes that:

- All footings are founded in controlled fill (if applicable) or in the residual clayey soils or rock below all non-controlled fill, topsoil material and root zones, and fill under slab panels meets the requirements of AS2870-2011, in particular, the root zone must be removed prior to the placement of fill materials beneath slabs.
- The performance expectations set out in Appendix B of AS2870-2011 are acceptable, and that site foundation maintenance is undertaken to avoid extremes of wetting and drying.
- Footings are to be founded outside of or below all zones of influence resulting from existing
 or future service trenches.
- The constructional and architectural requirements for reactive clay sites set out in AS2870-2011 are followed.
- Adherence to the detailing requirement outlined in Section 5 of AS2870-2011 'Residential Slabs and Footings' is essential, in particular Section 5.6, 'Additional requirements for Classes M, H1, H2 and E sites' including architectural restrictions, plumbing and drainage requirements.
- Site maintenance complies with the provisions of CSIRO Sheet BTF 18, "Foundation Maintenance and Footing Performance: A Homeowner's Guide", a copy of which is attached in Appendix C.

All structural elements on all lots regardless of their site classification should be supported on footings founded beneath all uncontrolled fill, layers of inadequate bearing capacity, soft/loose, or other potentially deleterious material.

If any areas of uncontrolled fill of depths greater than 0.4m are encountered during construction, footings should be designed in accordance with engineering principles for Class 'P' sites.

7.0 Limitations

The findings presented in the report and used as the basis for recommendations presented herein were obtained using normal, industry accepted geotechnical design practices and standards. To our knowledge, they represent a reasonable interpretation of the general conditions of the site.

The extent of testing associated with this assessment is limited to discrete test pit locations. It should be noted that subsurface conditions between and away from the test pit locations may be different to those observed during the field work and used as the basis of the recommendations contained in this report.

If subsurface conditions encountered during construction differ from those given in this report, further advice should be sought without delay.

Data and opinions contained within the report may not be used in other contexts or for any other purposes without prior review and agreement by Qualtest. If this report is reproduced, it must be in full.

If you have any further questions regarding this report, please do not hesitate to contact Shannon Kelly or the undersigned.

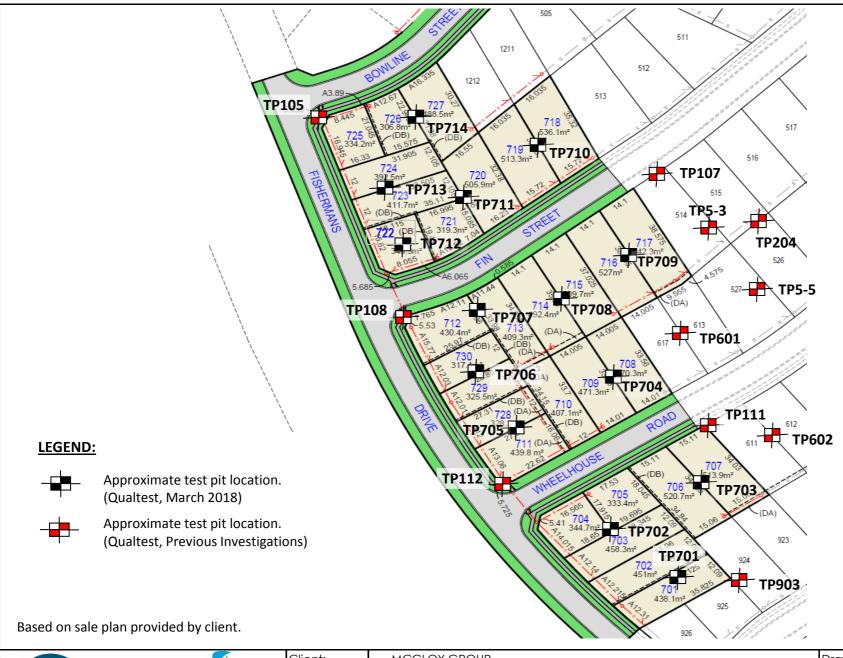
For and on behalf of Qualtest Laboratory (NSW) Pty Ltd.

Jason Lee

Principal Geotechnical Engineer



Figure AK1 –Approximate Test Pit Location Plan





Q	ualtest	
	LABORATORY (NSW) PTY LTD	

Client:	MCCLOY GROUP	Drawing No:	FIGURE AK1
Project:	PROPOSED SUBDIVISION - BILLY'S LOOKOUT - STAGE 7	Project No:	NEW15P-0070A
Location:	FISHERMANS DRIVE, TERALBA	Scale:	N.T.S.
Title:	APPROXIMATE TEST PIT LOCATION PLAN	Date:	27 MARCH 2018

APPENDIX A:

Engineering Logs of Test Pits



CLIENT: McCLOY GROUP

PROJECT: PROPOSED SUBDIVISION - STAGE 7

LOCATION: FISHERMANS DRIVE, TERALBA

LOGGED BY: ΒE DATE: 6-3-18

TP701

1 OF 1

NEW15P-0070A

TEST PIT NO:

PAGE:

JOB NO:

		IENT TYPE T LENGTH		5 TON 2.0 m				SURFA DATUM	JRFACE RL: ATUM:					
Drilling and Sampling			g and Sampling Material description and profile information				profile information	Fiel				d Test		
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION characteristics, colo	N: Soil type, plasticity/p ur,minor components	particle	MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations
E	Not Encountered	0.80m D 1.00m		- 0.5 		CL SC CH	FILL: Tree Mulch FILL: TOPSOIL - Sand plasticity, dark grey to a sand, trace fine to med gravel. Clayey SAND - fine to to red-brown and pale grained sub-angular gr Silty CLAY - medium to pale orange-brown, wit weathered rock.	dark brown, fine to coal itum grained sub-angul coarse grained, orange grey, with fine to coarse avel, trace cobbles.	rse lar 	D - M	MD - D	HP	350	FILL: TREE MULCH FILL: TOPSOIL RESIDUAL SOIL
				2.0	<u> </u>		2.00m Hole Terminated at 2.0	0 m						
Wate	Wat (Dat Wat	er Level e and time sh er Inflow	own)	Notes, Sar U ₅₀ CBR E ASS	50mm Bulk s Enviro (Glass Acid S	Diame ample f nmenta jar, sea ulfate S	er tube sample or CBR testing I sample aled and chilled on site) oil Sample		S S F Fi St S VSt V	ery Soft oft irm tiff ery Stiff		25 50 10 20	CS (kPe 25 5 - 50 0 - 100 00 - 200 00 - 400	D Dry M Moist W Wet D W _p Plastic Limit
	ta Cha Gi tra De	er Outflow Inges radational or Insitional stratefinitive or distertate change		B Field Test PID DCP(x-y) HP	Bulk S s Photoi Dynan	ample onisationic pene	ir expelled, chilled) n detector reading (ppm) strometer test (test depth interva meter test (UCS kPa)			ard riable V L MI D VD	Lo D D	ery Lo	n Dense	Density Index <15% Density Index 15 - 35% Density Index 35 - 65% Density Index 65 - 85% Density Index 85 - 100%



Gradational or

strata change

transitional strata

Definitive or distict

PID

HP

DCP(x-y)

Photoionisation detector reading (ppm)

Hand Penetrometer test (UCS kPa)

Dynamic penetrometer test (test depth interval shown)

ENGINEERING LOG - TEST PIT

CLIENT: McCLOY GROUP

PROJECT: PROPOSED SUBDIVISION - STAGE 7

LOCATION: FISHERMANS DRIVE, TERALBA

PAGE: 1 OF 1 JOB NO: NEW15P-0070A

TP702

LOGGED BY: BE

DATE: 6-3-18

TEST PIT NO:

Loose

Medium Dense

Very Dense

MD

VD

D

Density Index 15 - 35%

Density Index 35 - 65%

Density Index 65 - 85%

Density Index 85 - 100%

EQUIPMENT TYPE: 5 TONNE EXCAVATOR SURFACE RL: **TEST PIT LENGTH:** 2.0 m WIDTH: DATUM: Field Test Drilling and Sampling Material description and profile information CLASSIFICATION SYMBOL CONSISTENCY DENSITY MOISTURE CONDITION GRAPHIC LOG Test Type Structure and additional METHOD Result DEPTH MATERIAL DESCRIPTION: Soil type, plasticity/particle observations SAMPLES (m) (m) characteristics, colour, minor components М FILL: TREE MULCH FILL: Tree Mulch FILL: TOPSOIL FILL: TOPSOIL - Sandy CLAY - low to medium plasticity, brown to dark brown with some orange-brown, trace fine to medium grained 0.10m Š CL Σ D 0.20m sub-angular gravel. ΗP Not Encountered 180 COLLUVIUM / POSSIBLE FILL SAND - fine to coarse grained, dark grey, with some fine to medium grained sub-angular gravel, with 250 SP MD ш some clay pockets, medium to high plasticity. 0.40m Clayey SAND - fine to coarse grained, orange-brown and pale grey, medium plasticity, with sub-angular RESIDUAL SOIL Μ gravel. D MD SC 0.60m SANDSTONE - fine to coarse grained, pale grey and pale brown, estimated medium to high strength.

Hole Terminated at 0.71 m HIGHLY WEATHERED ROCK Refusal 1.0 <<DrawingFile>> 20-03-2018 11:48 10.0.000 Datgel Lab and In Situ Tool 1.5 TEST PIT NEW15P - 0070A LOGS - STAGE 7 & 12.GPJ 2.0 LEGEND: Moisture Condition Notes, Samples and Tests Consistency UCS (kPa) Very Soft 50mm Diameter tube sample U۵ VS <25 D Dry Water Bulk sample for CBR testing CBR S 25 - 50 Moist Soft М Water Level Ε Environmental sample F Firm 50 - 100 W Wet (Date and time shown) (Glass jar, sealed and chilled on site) St Stiff 100 - 200 W, Plastic Limit Water Inflow ASS Acid Sulfate Soil Sample VSt Very Stiff 200 - 400 W_L Liquid Limit Ż ■ Water Outflow (Plastic bag, air expelled, chilled) Н Hard >400 В Bulk Sample Fb Friable Strata Changes Ę Field Tests **Density** Very Loose Density Index <15%



CLIENT: McCLOY GROUP

PROJECT: PROPOSED SUBDIVISION - STAGE 7

LOCATION: FISHERMANS DRIVE, TERALBA

DATE: 6-3-18

TEST PIT NO:

LOGGED BY:

PAGE:

JOB NO:

TP703

1 OF 1

ΒE

NEW15P-0070A

		IENT TYPE: T LENGTH:		5 TON 2.0 m		DTH:	0.3 m DATE	FACE RL: UM:					
	Drill	ing and Samp	oling				Material description and profile information				Fiel	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticil characteristics,colour,minor componer		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additiona observations
ш	Not Encountered	0.05m D 0.20m		_		CL	FILL: Tree Mulch FILL: Sandy CLAY - low to medium plastic to dark brown and grey, fine to coarse grai	ned sand.	M < M		HP	180	FILL: TREE MULCH FILL: TOPSOIL FILL
	o N	D 0.40m		0.5		CI	grained, oránge-brown and pale grey. 0.40m 0.41m SANDSTONE - fine to coarse grained, pale pale brown, estimated medium to high stre	 e grey and /	∑ D				HIGHLY WEATHERED -
				0.5_			Hole Terminated at 0.41 m Refusal	rigui.					
				-									
				1. <u>0</u>									
				_									
				1.5									
				-									
				2. <u>0</u>									
				-									
1.50	- FAIR			-		-47.		l on white				00.00	A Maintain Continue
Wate	Wat (Dat Wat	er Level e and time sho er Inflow er Outflow	own)	Notes, Sar U ₅₀ CBR E ASS	50mm Bulk sa Enviro (Glass Acid S (Plasti	Diame ample f nmenta jar, se ulfate S c bag, a	Seter tube sample or CBR testing all sample aled and chilled on site) Soil Sample air expelled, chilled)	S S F F St S VSt V	Very Soft Soft Firm Stiff Very Stiff		25 50 10 20	CS (kPa 25 5 - 50 0 - 100 00 - 200 00 - 400 400	D Dry M Moist W Wet W _p Plastic Limit
Stra	G tra De	anges radational or ansitional strata efinitive or disti rata change	a -	B Field Tests PID DCP(x-y) HP	Photoi Dynan	onisatio	on detector reading (ppm) etrometer test (test depth interval shown) meter test (UCS kPa)	Fb F Density	Friable V L MD D VD	Lo M D	ery Lo oose lediun ense ery D	n Dense	Density Index <15% Density Index 15 - 35% Density Index 35 - 65% Density Index 65 - 85% Density Index 85 - 100%



CLIENT: McCLOY GROUP

PROJECT: PROPOSED SUBDIVISION - STAGE 7

LOCATION: FISHERMANS DRIVE, TERALBA

LOGGED BY: BE
DATE: 6-3-18

TEST PIT NO:

PAGE:

JOB NO:

TP704

1 OF 1

NEW15P-0070A

		IT LENGT		2.0 m		IDTH:		M:					
	Dril	ling and San	npling				Material description and profile information				Field	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity characteristics,colour,minor component		MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations
		0.05m D 0.15m 0.20m		-		CL	0.04m FILL: Tree Mulch FILL: TOPSOIL - Sandy CLAY - low to med plasticity, dark grey to dark brown, fine to co 0.18m grained sand, trace fine to medium grained sub-angular gravel.	oarse	M < W		HP	280	FILL: TREE MULCH FILL: TOPSOIL RESIDUAL SOIL
Е	Not Encountered	D 0.40m		- 0. <u>5</u> -		SC	Clayey SAND - fine to coarse grained, pale orange-brown to red-brown, with highly wea pockets, with fine to coarse grained sub-angravel, fines of medium plasticity.	thered	D - M	MD - D		>000	RESIDUAL SOIL
				_	//		0.80m O.81m SANDSTONE - fine to coarse grained, red-	 brown, /	D /				HIGHLY WEATHERED
				1.0			estimated medium to high strength. Hole Terminated at 0.81 m Refusal						
				- - - 2.0_									
<u>Wat</u>	 Wat (Da	ter Level te and time si	nown)	Notes, Sal U ₅₀ CBR E	50mm Bulk s Enviro (Glass	Diame ample nment jar, se	ter tube sample for CBR testing al sample aled and chilled on site)	S S F F St S	ery Soft oft irm tiff		-25 50 10	CS (kPa 25 6 - 50 0 - 100 00 - 200 00 - 400	D Dry M Moist W Wet W _p Plastic Limit
-	l Wat ta Ch G tra D	ter Outflow anges irradational or ansitional stra efinitive or dis irrata change	ıta	B Field Test PID DCP(x-y) HP	(Plasti Bulk S <u>s</u> Photoi Dynan	c bag, ample onisati nic pen	Soil Sample air expelled, chilled) on detector reading (ppm) etrometer test (test depth interval shown) ometer test (UCS kPa)	н н	ery Stiff lard riable V L MD D VD	Lo M De	ery Lo	oose n Dense	W _L Liquid Limit Density Index <15% Density Index 15 - 35% Density Index 35 - 65% Density Index 65 - 85% Density Index 85 - 100%



CLIENT: McCLOY GROUP

PROJECT: PROPOSED SUBDIVISION - STAGE 7

LOCATION: FISHERMANS DRIVE, TERALBA

LOGGED BY: BE
DATE: 6-3-18

TP705

1 OF 1

NEW15P-0070A

TEST PIT NO:

PAGE:

JOB NO:

		IENT TYPE T LENGTH		5 TON 2.0 m		(CAV) I DTH :		RFACE RL: TUM:					
		ing and Sam					Material description and profile information				Field	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plastic characteristics,colour,minor compone		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations
Е	Encountered	0.10m D		_		CL	FILL: Tree Mulch FILL: TopSoIL - Sandy CLAY - low to m plasticity, dark grey to dark brown, with so fine to coarse grained sand, trace fine to	me orange	M ~ % ~ W				FILL: TREE MULCH FILL: TOPSOIL
	Not Er	<u>0.20m</u>		1.6			grained sub-angular gravel. SANDSTONE - fine to coarse grained, pared-brown and pale grey, estimated medistrength. Hole Terminated at 0.21 m Refusal						HIGHLY WEATHERED ROCK
Wat	Wat (Dat Wat Wat		own)	Notes, Sal U ₅₀ CBR E ASS B	50mm Bulk s Enviro (Glass Acid S (Plasti Bulk S	Diame ample f nmenta jar, se ulfate S c bag, a	ts ter tube sample for CBR testing al sample aled and chilled on site) Soil Sample air expelled, chilled)	S S F F St S VSt \ H F	Very Soft Soft Firm Stiff Very Stiff Hard Friable		25 50 10 20 >4	5 - 50 0 - 100 00 - 200 00 - 400	D Dry M Moist W Wet W _p Plastic Limit W _L Liquid Limit
	tra De	radational or ansitional strata efinitive or dist rata change	а	Field Test PID DCP(x-y) HP	Photoi Dynan	nic pen	on detector reading (ppm) etrometer test (test depth interval shown) ometer test (UCS kPa)	<u>Density</u>	V L MC D VD	Lo M D	ery Lo pose ledium ense ery De	n Dense	Density Index <15% Density Index 15 - 35% Density Index 35 - 65% Density Index 65 - 85% Density Index 85 - 100%



CLIENT: McCLOY GROUP

PROJECT: PROPOSED SUBDIVISION - STAGE 7

LOCATION: FISHERMANS DRIVE, TERALBA

LOGGED BY: BE
DATE: 6-3-18

TP706

1 OF 1

NEW15P-0070A

TEST PIT NO:

PAGE:

JOB NO:

TE	ST P	IT LENGTH	1 :	2.0 m	W	IDTH:	0.3 m DAT U	JM:					
	Dril	ling and San	npling				Material description and profile information				Field	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticit characteristics,colour,minor componen		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations
	ntered			-		sc	FILL: Tree Mulch FILL: TOPSOIL - Clayey SAND - fine to co grained, dark grey to dark brown, fines of k medium plasticity.	arse ow to	M				FILL: TREE MULCH FILL: TOPSOIL
Ш	Not Encountered	0.30m D 0.50m		- 0. <u>5</u>	XXX /// /// ///	SC	Clayey SAND - fine to coarse grained, pale orange-brown and pale grey, with fine to cograined sub-angular gravel.	oarse	D - M	D			RESIDUAL SÕIL
				_	/ :/::		0.60m O.610r SANDSTONE - fine to coarse grained, pale pale red-brown, estimated medium to high	grey and	D.				HIGHLY WEATHERED
				_			Hole Terminated at 0.61 m Refusal	ouongui.					
				-									
				1.0_									
				-									
				_									
				1. <u>5</u>									
				-									
				-									
				-									
				2.0_									
				_									
				_									
				-									
													N
Wat	_			Notes, Sa U ₅₀ CBR	50mm	Diame	<u>ts</u> ter tube sample for CBR testing	1	ncy ′ery Soft Soft		<2	CS (kPa 25 5 - 50	Moisture Condition D Dry M Moist
<u> </u>	(Da	ter Level te and time sh ter Inflow	nown)	E ASS	Enviro (Glass Acid S	onmenta s jar, se Sulfate S	al sample aled and chilled on site) Soil Sample	F F St S VSt V	irm Stiff ery Stiff		50 10 20) - 100)0 - 200)0 - 400	W Wet W _p Plastic Limit
Stra		ter Outflow anges		В	Bulk S	ic bag, Sample	air expelled, chilled)	Fb F	lard riable			100	
_	tra D	radational or ansitional stra efinitive or dis	ıta	Field Test PID DCP(x-y) HP	Photo Dynar	nic pen	on detector reading (ppm) etrometer test (test depth interval shown) ometer test (UCS kPa)	<u>Density</u>	V L ME D	Lo D M	ery Lo oose lediun ense	oose n Dense	Density Index <15% Density Index 15 - 35% Density Index 35 - 65% Density Index 65 - 85%
	SI	rata change							VD		ery D	ense	Density Index 85 - 100%



CLIENT: McCLOY GROUP

PROJECT: PROPOSED SUBDIVISION - STAGE 7

LOCATION: FISHERMANS DRIVE, TERALBA

LOGGED BY: BE
DATE: 6-3-18

TP707

1 OF 1

NEW15P-0070A

TEST PIT NO:

PAGE:

JOB NO:

		IENT TYPE		5 TON 2.0 m		IDTH:		FACE RL: JM:					
	Drill	ling and Sam	pling				Material description and profile information				Field	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticit characteristics,colour,minor componen		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations
	Not Encountered			-		SC	FILL: Tree Mulch FILL: TOPSOIL - Clayey SAND - fine to co grained, dark grey to dark brown, fine to m sub-angular gravel, fines of low to medium root affected.	edium plasticity,					FILL: TREE MULCH FILL: TOPSOIL
Ш	Not En	0.60m D 0.70m		0. <u>5</u>		SP	Extremely Weathered Sandstone with soil breaks down into Gravelly Sand - fine to congrained, pale orange-brown and pale grey, highly weathered pockets.	arse	D - M	D			EXTREMELY WEATHERE ROCK
				_	0 0		0.75m 0.77m SANDSTONE - fine to coarse grained, pale		D				HIGHLY WEATHERED ROCK
				_			\pale red-brown, estimated low to medium s Hole Terminated at 0.77 m Refusal	strength.					IROCK
				1.0_			Neiusai						
				1.5									
				_									
				_									
				-									
				-									
				2.0_									
				-									
				-									
				-									
				-									
	END:			Notes, Sa			t <u>s</u> ter tube sample	Consister VS V	ncy ery Soft			 CS (kPa 25	Moisture Condition D Dry
Wat	_	ter Level		U ₅₀ CBR E	Bulk s	ample t	ter tube sample or CBR testing al sample	s s	ery Son oft irm		25	25 5 - 50 0 - 100	M Moist W Wet
—	•	te and time sh ter Inflow	1	ASS	(Glass	s jar, se	aled and chilled on site) Soil Sample	St S	tiff 'ery Stiff		10) - 100)0 - 200)0 - 400	W _p Plastic Limit
Stra		ter Outflow anges		В	(Plast		air expelled, chilled)	н н	lard riable		>4	100	
	G	radational or ansitional strat	ta	Field Test PID	Photo		on detector reading (ppm)	<u>Density</u>	V L	Lo	ery Lo		Density Index <15% Density Index 15 - 35%
-	D	efinitive or dis rata change		DCP(x-y) HP			etrometer test (test depth interval shown) ometer test (UCS kPa)		ME D	D	ense	n Dense	Density Index 65 - 85%
									VD	V	ery D	ense	Density Index 85 - 100%



CLIENT: McCLOY GROUP

PROJECT: PROPOSED SUBDIVISION - STAGE 7

LOCATION: FISHERMANS DRIVE, TERALBA

LOGGED BY: DATE:

TEST PIT NO:

PAGE:

JOB NO:

TP708

1 OF 1

ΒE

6-3-18

NEW15P-0070A

TES	ST PI	T LENGTH	1 :	2.0 m	W	IDTH:	0.3 m DATU	JM:					
	Drill	ing and Sam	npling				Material description and profile information				Field	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticit characteristics,colour,minor componen		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations
Е	Not Encountered	0.30m		-		CL SC	FILL: Tree Mulch FILL: TOPSOIL - Sandy CLAY - low to med plasticity, dark brown with some dark grey, coarse grained sand, with some fine to me grained sub-angular gravel. 0.25m Clayey SAND - fine to coarse grained, pale orange-brown to red-brown and pale grey, low to medium plasticity, fine to medium graub-angular to angular gravel.	fine to dium ————— fines of ained	D-M × × ×	MD -			FILL: TREE MULCH FILL: TOPSOIL RESIDUAL SOIL EXTREMELY WEATHEREI ROCK
		0.50m		0.5_		SP	Extremely weathered Sandstone with soil preaks down into Gravelly Sand - fine to congrained, pale grey and pale orange, fine to angular to sub-angular gravel, trace clay. O.65m O.65m O.65m O.65m	oarse coarse	D - M	D - VD			HIGHLY WEATHERED
				_			SANDSTONE - fine to coarse grained, pale pale red-brown, estimated low to medium s Hole Terminated at 0.66 m Refusal	e grey and strength.					ROCK
				1. <u>0</u>									
				_									
				_									
				-									
				1. <u>5</u>									
				_									
				_									
				-									
				2.0									
				_									
				-									
				-									
LEG	SEND:			Notes, Sa				Consiste		<u> </u>	_	CS (kPa	
Wat		or Level		U₅₀ CBR			ter tube sample or CBR testing	1	ery Soft Oft			25 5 - 50	D Dry M Moist
<u>+</u>	(Dat	er Level e and time sh er Inflow	1	E ASS	Enviro (Glass	nmenta jar, se	al sample aled and chilled on site) Soil Sample	St S	irm Stiff ery Stiff		10	0 - 100 00 - 200 00 - 400	P
Ctro		er Outflow		В	(Plasti		air expelled, chilled)	н н	lard riable			400	
<u>Stra</u>	 tra	radational or ansitional stra	ita	Field Test PID	<u>s</u> Photoi	onisatio	on detector reading (ppm)	<u>Density</u>	V L	Lo	ery Lo		Density Index <15% Density Index 15 - 35%
		efinitive or dis rata change	stict	DCP(x-y) HP	-		etrometer test (test depth interval shown) ometer test (UCS kPa)		ME D VD	D	ediun ense ery Do	n Dense ense	Density Index 35 - 65% Density Index 65 - 85% Density Index 85 - 100%



CLIENT: McCLOY GROUP

PROJECT: PROPOSED SUBDIVISION - STAGE 7

LOCATION: FISHERMANS DRIVE, TERALBA

LOGGED BY: BE
DATE: 6-3-18

TP709

1 OF 1

NEW15P-0070A

TEST PIT NO:

PAGE:

JOB NO:

		IENT TYPE: T LENGTH:	5 TOI 2.0 m	(A BUN W	(CAV) I DTH :		RFACE RL:					
		ing and Sampli				Material description and profile information				Field	d Test	
METHOD	WATER		RL DEPTH	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plas characteristics,colour,minor compo		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations
ш	Not Encountered					FILL: Tree Mulch FILL: TOPSOIL - Sandy CLAY - low to plasticity, dark brown with some dark groanse grained sand, with some fine to grained sub-angular gravel. Extremely weathered Sandstone with s	ey, fine to medium — — — — —/	M				FILL: TREE MULCH FILL: TOPSOIL EXTREMELY WEATHERE
			1.6			breaks down into Gravelly Sand - fine to grained, pale grey and pale orange, fine angular to sub-angular gravel, trace class SANDSTONE - fine to coarse grained, pale red-brown, estimated low to mediu. Hole Terminated at 0.33 m Practical Refusal	coarse /coarse					HIGHLY WEATHERED ROCK
<u>Wat</u>	Wat (Dat Wat Wat ta Cha	er Level e and time show er Inflow er Outflow anges radational or ansitional strata	ASS B Field Tes	50mm Bulk s Enviro (Glass Acid S (Plasti Bulk S	n Diame sample formenta s jar, sea Sulfate S ic bag, a Sample	ter tube sample or CBR testing al sample aled and chilled on site) Soil Sample air expelled, chilled) on detector reading (ppm) etrometer test (test depth interval shown)	S S F F St S VSt V	vncy /ery Soft Soft Firm Stiff /ery Stiff Hard Friable V L	Vi Lo	25 50 10 20 20 20 ery Lo	CS (kPa) 25 5 - 50 0 - 100 00 - 200 00 - 400 400 pose	D Dry M Moist W Wet W _p Plastic Limit W _L Liquid Limit Density Index <15% Density Index 15 - 35%



CLIENT: McCLOY GROUP

PROJECT: PROPOSED SUBDIVISION - STAGE 7

LOCATION: FISHERMANS DRIVE, TERALBA

LOGGED BY: BE
DATE: 6-3-18

TP710

1 OF 1

NEW15P-0070A

TEST PIT NO:

PAGE:

JOB NO:

	Drill	ing and Sam	pling				Material description and profile information				Fiel	d Test	
METHOD	WATER	SAMPLES		DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticil characteristics, colour, minor componer		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additiona observations
ш	Not Encountered			-		SP	Extremely weathered Sandstone with soil preaks down into Gravelly Sand - fine to congrained, pale grey and pale orange, fine to angular to sub-angular gravel, trace clay.	arse		D - VD)		EXTREMELY WEATHERE ROCK
				-			SANDSTONE - fine to coarse grained, pale red-brown, estimated medium to high	e grey and strength.	-				HIGHLY WEATHERED ROCK
				_			Hole Terminated at 0.28 m Refusal						
				0.5									
				_									
				1.0									
				1.5									
				1.5_									
				_									
				-									
				2.0_									
				-									
				-									
				-									
				-									
	END:		1	Notes, Sar			ts ter tube sample	Consiste VS V	ncy /ery Soff	<u> </u>		CS (kPa 25	Moisture Condition D Dry
Wate		er Level		CBR E	Bulk s	ample f	or CBR testing al sample	s s	Soft Firm	-	25	5 - 50 0 - 100	M Moist W Wet
_	Wat	e and time sh er Inflow	´	ASS	(Glass	jar, se	aled and chilled on site) Soil Sample	St S	 Stiff /ery Stiff	Ŧ	10	00 - 200 00 - 400	W _p Plastic Limit
- Stra	Wat	er Outflow anges		В	(Plasti Bulk S	c bag, a	air expelled, chilled)	H F	lard riable		>4	400	
	Gi	radational or ansitional strat	ta l	Field Test	Photoi		on detector reading (ppm)	Density	V L	Lo	ery Lo		Density Index <15% Density Index 15 - 35%
	_ De	efinitive or dist		DCP(x-y) HP			etrometer test (test depth interval shown) ometer test (UCS kPa)		ME D		lediun ense	n Dense	Density Index 35 - 65% Density Index 65 - 85%



CLIENT: McCLOY GROUP

PROJECT: PROPOSED SUBDIVISION - STAGE 7

LOCATION: FISHERMANS DRIVE, TERALBA

LOGGED BY: BE
DATE: 6-3-18

TP711

1 OF 1

NEW15P-0070A

TEST PIT NO:

PAGE:

JOB NO:

		IENT TYPE T LENGTH:		5 TON 2.0 m		(CAV. I DTH :		FACE RL: JM:					
	Drill	ing and Samp	oling				Material description and profile information				Field	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticit characteristics,colour,minor componer	y/particle ts	MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations
		0.10m D 0.20m		-		SC	FILL: TOPSOIL - Clayey SAND - fine to co grained, pale orange-brown to red-brown a grey, fines of low to medium plasticity, fine grained sub-angular to angular gravel.	arse ind pale to medium	D - M				FILL: TOPSOIL
ш	Not Encountered	D 0.60m		- 0.5 1.0		СН	Extremely weathered Sandstone with soil preaks down into Silty Clay - medium to his plasticity, pale grey and pale orange, with his weathered pockets.	ah [*]	M < Wp	Н			EXTREMELY WEATHERE ROCK
				- 1. <u>5</u> - - 2.0_			1.35m SANDSTONE - fine to coarse grained, pall pale red-brown, estimated low to medium s Hole Terminated at 1.35 m Refusal	e grey and etrength.	D				HIGHLY WEATHERED ROCK
Wat	Wat (Dat Wat Wat I Wat Gata Cha Itra	er Level te and time sho er Inflow er Outflow anges randational strata efinitive or disti	own)	Notes, Sai U ₅₀ CBR E ASS B Field Test PID DCP(x-y)	50mm Bulk s Enviro (Glass Acid S (Plasti Bulk S S Photoi Dynan	Diame ample in nmenta i jar, se sulfate s c bag, ample onisationic pen	ts Inter tube sample Inter tub	S S F F St S VSt V	very Soft Firm Stiff Very Stiff Hard Friable V L ME D	V L(25 50 10 20 20 20 ery Lo	n Dense	D Dry M Moist W Wet W _p Plastic Limit W _L Liquid Limit Density Index <15% Density Index 15 - 35%



CLIENT: McCLOY GROUP

PROJECT: PROPOSED SUBDIVISION - STAGE 7

LOCATION: FISHERMANS DRIVE, TERALBA

PAGE: 1 OF 1

TEST PIT NO:

LOGGED BY:

JOB NO: NEW15P-0070A

TP712

ΒE

DATE: 6-3-18

		IT LENGTH		2.0 m		DTH:	0.3 m DAT	JM:					
	Dril	ling and Samp	oling				Material description and profile information				Field	d Test	
МЕТНОБ	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plastici characteristics,colour,minor componer		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations
tu Tool	Not Encountered	0.30m D 0.50m		- 0.5 - - - 1.0		SC SP SP CH	0.03m FILL: Tree Mulch FILL: TOPSOIL - Clayey SAND - fine to compare fine death of the compared of the compare	ow to ed, grey, sined, rown and egrey and	D - M	Н	HP	>600	FILL: TREE MULCH FILL: TOPSOIL FILL RESIDUAL SOIL
OT LIB 1.1.G.IB Log NON-CORED BOREHOLE. TEST PIT NEW15P0070A LOGS - STAGE 7 & 12.GPJ < <drawingfile>> 20-03-2018 11:49 10.0.000 Datgel Lab and In Situ Tool</drawingfile>				1.5			1.10m SANDSTONE - fine to coarse grained, pal pale red-brown, estimated low to medium : Hole Terminated at 1.15 m Refusal		D				HIGHLY WEATHERED ROCK
QT LIB 1.1.GLB Log NON-CORED BOREHOLE - TI	(Da — Wa ■ Wa rata Ch — G tr — D	ter Level te and time sho ter Inflow ter Outflow	own) A	otes, Sai U ₅₀ BR E SS B ield Test PID CP(x-y) HP	50mm Bulk sa Enviro (Glass Acid S (Plasti Bulk S Photoi Dynan	Diame ample from the sample fr	er tube sample or CBR testing I sample aled and chilled on site) oil Sample iir expelled, chilled) in detector reading (ppm) etrometer test (test depth interval shown) meter test (UCS kPa)	S S F F St S VSt V H H	lery Soft oft irm tiff ery Stiff ard riable V L MC D VD	V(Lc) M	25 50 10 20 20 20 ery Lo	5 - 50 0 - 100 00 - 200 00 - 400 400 pose	D Dry M Moist W Wet W _p Plastic Limit W _L Liquid Limit Density Index <15% Density Index 15 - 35%



CLIENT: McCLOY GROUP

PROJECT: PROPOSED SUBDIVISION - STAGE 7

LOCATION: FISHERMANS DRIVE, TERALBA

LOGGED BY: BE
DATE: 6-3-18

TEST PIT NO:

PAGE:

JOB NO:

TP713

1 OF 1

NEW15P-0070A

163		IT LENGTH		2.0 m	W	IDTH:	0.3 m	DATUM:			F	. .	
	Dril	ling and Sam					Material description and profile info	mation			Fiel	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type characteristics,colour,minor co		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additiona observations
	peu						0.05m FILL: Tree Mulch						FILL: TREE MULCH
Е	Not Encountered			_		sc	FILL: TOPSOIL - Clayey SAND - 1 grained, pale grey, root affected.		D - M				FILL: TOPSOIL
							0.30m SANDSTONE - fine to coarse grain pale red-brown, estimated medium	ned, pale grey and n to high strength.	D				HIGHLY WEATHERED ROCK
				_			Hole Terminated at 0.30 m Refusal						
				0.5									
				-									
				-									
				-									
				_									
				1.0									
				_									
				-									
				-									
				_									
				1.5_									
				-									
				-									
				_									
				_									
				2.0									
				-									
				-									
				-									
LEC	END			Note: C:	mmle -	ad Teef		0				CC /I-D	Meintura Countition
Wat	END: <u>er</u>			Notes, Sar	50mm	Diamet	er tube sample		Very Sof	t	<2	CS (kPa 25	D Dry
Y		ter Level te and time sh		CBR E	Enviro	nmenta	or CBR testing	F	Soft Firm		50	5 - 50 0 - 100	M Moist W Wet
—	Wat	ter Inflow	1	ASS	Acid S	ulfate S	aled and chilled on site) oil Sample	VSt '	Stiff Very Stiff	Ŧ	20	00 - 200 00 - 400	P
- Stra		er Outflow anges		В		c bag, a ample	ir expelled, chilled)	I	Hard Friable		>4	400	
	G	radational or ansitional strat		Field Test PID	_	onisatio	n detector reading (ppm)	<u>Density</u>	V L		ery Lo oose	oose	Density Index <15% Density Index 15 - 35%
	_ D	efinitive or dist		DCP(x-y) HP	Dynan	nic pene	etrometer test (test depth interval shown) meter test (UCS kPa)		MI D		lediun ense	n Dense	
	st	rata change			and	55			VE		ery D	ense	Density Index 85 - 100%



CLIENT: McCLOY GROUP

PROJECT: PROPOSED SUBDIVISION - STAGE 7

LOCATION: FISHERMANS DRIVE, TERALBA

LOGGED BY: ΒE DATE: 6-3-18

TP714

1 OF 1

NEW15P-0070A

TEST PIT NO:

PAGE:

JOB NO:

		IENT TYPE T LENGTH		5 TON 2.0 m		(CAV. I DTH :		SURFA DATUM						
	Drill	ing and Sam	pling				Material description and	d profile information				Field	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTIC characteristics,col	DN: Soil type, plasticity/p our,minor components	particle	MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations
				-		SM	grained, pale grey, fine root affected.	ey SAND - Fine to coanses of low to medium pla	se sticity,	D - M				FILL: TREE MULCH FILL: TOPSOIL
Е	Not Encountered	0.30m D 0.50m		- 0. <u>5</u> -			breaks down into Silty plasticity, pale grey an		— — — - perties:					EXTREMELY WEATHERED ROCK
	Not			- 1. <u>0</u> - -		CH	with highly weathered	sandstone pockets.		M < Wp	н			
				1. <u>5</u>			Hole Terminated at 1. Very slow progress	40 m						
				2.0_										
				-										
<u>Wat</u>	Wat (Dat Wat Wat	er Level e and time sh er Inflow er Outflow		Notes, Sal U ₅₀ CBR E ASS	50mm Bulk s Enviro (Glass Acid S (Plasti	Diame ample to nmenta jar, se sulfate s	ter tube sample or CBR testing all sample aled and chilled on site) soil Sample air expelled, chilled)		S S F F St S VSt V H H	ncy /ery Soft /oft /irm /ery Stiff /ery Stiff /ard		25 50 10 20	CS (kPa 25 5 - 50 0 - 100 00 - 200 00 - 400 400	D Dry M Moist W Wet W _p Plastic Limit
<u>stra</u>	tra De	anges radational or ansitional strat efinitive or dist rata change		Field Test PID DCP(x-y) HP	<u>:s</u> Photoi Dynan	onisatio	on detector reading (ppm) etrometer test (test depth interva meter test (UCS kPa)		Density	V L ME D VD	Lo N D	ery Lo oose lediun ense ery De	n Dense	Density Index <15% Density Index 15 - 35% Density Index 35 - 65% Density Index 65 - 85% Density Index 85 - 100%



CLIENT: MCCLOY GROUP DEVELOPMENT MANAGEMENT PPAGED

PROJECT: PROPOSED SUBDIVISION - STAGES 5 TO 9 JOB NO: NEW15P-0070A

LOCATION: PITT STREET, TERALBA LOGGED BY: SJK

DATE: 13-1-16

TEST PIT NO:

TP105

1 OF 1

EQUIPMENT TYPE: 22 tonne excavator SURFACE RL: 39.0 m **TEST PIT LENGTH:** 3.0 m WIDTH: 1.5 m DATUM: Assumed Field Test Drilling and Sampling Material description and profile information CLASSIFICATION SYMBOL CONSISTENCY DENSITY MOISTURE CONDITION GRAPHIC LOG Test Type Structure and additional METHOD WATER Result DEPTH MATERIAL DESCRIPTION: Soil type, plasticity/particle observations SAMPLES (m) (m) characteristics, colour, minor components TOPSOIL / RESIDUAL SOIL CLAY - medium to high plasticity, pale brown, some fine to medium grained sand, root affected. CH HP 250 CLAY - medium to high plasticity, pale grey and pale brown, some fine to medium grained sand, trace of fine to coarse grained angular gravel (sandy RESIDUAL SOIL VSt 0.40m siltstone). 38.5 ΗP 270 U50 СН HP 450 0.80m Encountered 38.0 1.0 HIGHLY WEATHERED Sandy SILTSTONE - grey to pale grey with pale brown to orange, sand mostly fine grained, estimated low to medium strength, semi-fractured. **ROCK** ш Not TEST PIT NEW15P-0070 LOGS - STAGES 5 TO 9.GPJ <<DrawingFile>> 20-03-2018 13:33 10.0.000 Datgel Lab and In Situ Tool 37.5 1.5 М 37.0 Silty SANDSTONE - mostly fine grained, pale brown with grey, estimated medium strength. D Hole Terminated at 2 30 m Slow progress 2.5 36.5 LEGEND: Moisture Condition Notes, Samples and Tests Consistency UCS (kPa) 50mm Diameter tube sample Verv Soft U۵ VS <25 D Dry Water CBR Bulk sample for CBR testing S 25 - 50 Moist Soft М Water Level Ε Environmental sample F Firm 50 - 100 W Wet (Date and time shown) (Glass jar, sealed and chilled on site) St Stiff 100 - 200 W, Plastic Limit Water Inflow ASS Acid Sulfate Soil Sample VSt Very Stiff 200 - 400 W_L Liquid Limit ■ Water Outflow (Plastic bag, air expelled, chilled) Н Hard >400 В Bulk Sample Fb Friable Strata Changes Ę Field Tests **Density** Very Loose Density Index <15% Gradational or PID Photoionisation detector reading (ppm) Loose Density Index 15 - 35% transitional strata DCP(x-y) Dynamic penetrometer test (test depth interval shown) MD Medium Dense Density Index 35 - 65% Definitive or distict HP Hand Penetrometer test (UCS kPa) D Density Index 65 - 85% strata change VD Very Dense Density Index 85 - 100%



CLIENT: MCCLOY GROUP DEVELOPMENT MANAGEMENT PRAGED

PROJECT: PROPOSED SUBDIVISION - STAGES 5 TO 9 JOB NO: NEW15P-0070A

LOCATION: PITT STREET, TERALBA **LOGGED BY:** SJK

DATE: 12-1-16

TEST PIT NO:

TP107

1 OF 1

EQUIPMENT TYPE: 22 tonne excavator SURFACE RL: 34.5 m **TEST PIT LENGTH:** 3.0 m WIDTH: 1.5 m DATUM: Assumed Field Test Drilling and Sampling Material description and profile information CLASSIFICATION SYMBOL CONSISTENCY DENSITY MOISTURE CONDITION GRAPHIC LOG Test Type Structure and additional METHOD Result DEPTH MATERIAL DESCRIPTION: Soil type, plasticity/particle SAMPLES (m) (m) characteristics, colour, minor components TOPSOIL Silty SAND - fine to coarse grained, brown to grey, fines of low plasticity, root affected. SM Encountered CLAY - medium to high plasticity, pale brown to orange and pale grey, trace to some fine to medium grained sand. RESIDUAL SOIL СН VSt Š 34.0 0.5 HIGHLY WEATHERED Interbedded SILTSTONE and SANDSTONE - grey ROCK to pale grey with orange, fine to medium grained sand, estimated high strength, fractured. ᅙ Hole Terminated at 0.75 m Practical Refusal 33.5 1.0 TEST PIT NEW15P-0070 LOGS - STAGES 5 TO 9.GPJ <-DrawingFile>> 20-03-2018 13:33 10.0.000 Datgel Lab and In Situ Tool 33.0 1.5 32.5 2.0 2.5 32.0 NON-CORED BOREHOLE -LEGEND: Moisture Condition Notes, Samples and Tests Consistency UCS (kPa) 50mm Diameter tube sample Verv Soft U۵ VS <25 D Dry Water CBR Bulk sample for CBR testing S 25 - 50 Moist Soft М Water Level Ε Environmental sample F Firm 50 - 100 W Wet (Date and time shown) (Glass jar, sealed and chilled on site) St Stiff 100 - 200 W, Plastic Limit Water Inflow ASS Acid Sulfate Soil Sample VSt Very Stiff 200 - 400 W_L Liquid Limit ■ Water Outflow (Plastic bag, air expelled, chilled) Н Hard >400 В Bulk Sample Fb Friable Strata Changes Ę Field Tests **Density** Very Loose Density Index <15% Gradational or PID Photoionisation detector reading (ppm) Loose Density Index 15 - 35% transitional strata DCP(x-y) Dynamic penetrometer test (test depth interval shown) MD Medium Dense Density Index 35 - 65% Definitive or distict HP Hand Penetrometer test (UCS kPa) D Density Index 65 - 85% strata change VD Very Dense Density Index 85 - 100%



MCCLOY GROUP DEVELOPMENT MANAGEMENT P**PAGE**D

PROJECT: PROPOSED SUBDIVISION - STAGES 5 TO 9 **JOB NO**: NEW15P-0070A

LOCATION: PITT STREET, TERALBA

LOGGED BY: SJK

TEST PIT NO:

DATE:

TP108

1 OF 1

13-1-16

EQUIPMENT TYPE: 22 tonne excavator SURFACE RL: 35.0 m
TEST PIT LENGTH: 3.0 m WIDTH: 1.5 m DATUM: Assumed

		IENT TYP IT LENGTI		22 ton 3.0 m		avaio I DTH :		SURFACE RL: DATUM:		85.0 m Assum			
	Drill	ing and San	npling				Material description and profile info	rmation			Fiel	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type characteristics,colour,minor c	e, plasticity/particle omponents	MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations
			-	_		sc	Clayey SAND - fine to coarse gra grey, fines of low to medium plast grained gravel, root affected.		М				TOPSOIL
Ш	Not Encountered		- - 34. <u>5</u> -	0.5_		CH	CLAY / Sandy CLAY - medium to brown to orange with grey, fine to sand, some tree roots. 0.70m SANDSTONE - fine to medium gr	medium grained	M > W _P	St	HP	150	RESIDUAL SOIL HIGHLY WEATHERED
					: : : : :		0.80m to orange, pale grey to white and	brown to red,	D				ROCK
			34. <u>0</u>	1.0			∖estimated high strength. Hole Terminated at 0.80 m Refusal						
			33. <u>5</u>	-									
			- 32. <u>5</u> - - -	2.5_ 									
Wat	Wat (Dat Wat Wat	er Level te and time sl er Inflow er Outflow anges	nown)	Notes, San U ₅₀ CBR E ASS	50mm Bulk s Enviro (Glass Acid S (Plasti	Diame ample to nmenta jar, se sulfate s	is ter tube sample or CBR testing all sample aled and chilled on site) soil Sample air expelled, chilled)	S S F F St S VSt V H F	ncy /ery Soft foft firm stiff /ery Stiff lard friable		25 50 10 20	CS (kPa 25 5 - 50 0 - 100 00 - 200 00 - 400 400	D Dry M Moist W Wet W _p Plastic Limit
	G tra De	radational or ansitional stra efinitive or dis rata change	ıta	Field Test PID DCP(x-y) HP	<u>s</u> Photoi Dynan	onisatio	on detector reading (ppm) etrometer test (test depth interval shown) ometer test (UCS kPa)	Density	V L ME D VC	Lo D D	ery Lo oose lediun ense ery D	n Dense	Density Index <15% Density Index 15 - 35% Density Index 35 - 65% Density Index 65 - 85% Density Index 85 - 100%



MCCLOY GROUP DEVELOPMENT MANAGEMENT P**PAGE**D

PROJECT: PROPOSED SUBDIVISION - STAGES 5 TO 9 JOB NO: NEW15P-0070A

LOCATION: PITT STREET, TERALBA

LOGGED BY: SJK

TP111

1 OF 1

DATE: 12-1-16

TEST PIT NO:

EQUIPMENT TYPE: 22 tonne excavator SURFACE RL: 34.0 m

TE	ST PI	T LENGTI	H:	3.0 m	W	DTH:		TUM:	Ä	Assum	ned		
	Drilling and Sampling					Material description and profile information					d Test		
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plas characteristics,colour,minor compor		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations
	ered		_	_		sc	Clayey SAND - fine to coarse grained, or grey, fines of low to medium plasticity, to	ark brown to ace of fine	М				TOPSOIL
ш	Not Encountered		- - -			CI	o_15m grained gravel, root affected. Sandy CLAY - medium plasticity, pale b medium grained sand, some tree roots.	rown, fine to	M × W _P	St	HP	150	RESIDUAL SOIL
			33.5	0.5			0.50m SANDSTONE - fine to medium grained, and pale grey, estimated high strength.	pale brown	D				HIGHLY WEATHERED ROCK
			- - -				Hole Terminated at 0.50 m Refusal						
			33.0	1.0									
			-	_									
			-	_									
			-	_									
			32.5	1. <u>5</u>									
			-	_									
			-	_									
			-	-									
			32.0	2. <u>0</u>									
			-	_									
			-	_									
			-	_									
			31. <u>5</u>	2.5_									
			-	_									
			-	_									
			-	_									
					mples aı			Consiste				CS (kPa	-
Y	Water ✓ Water Level (Date and time shown) ✓ Water Inflow ✓ Water Outflow Strata Changes			U ₅₀ 50mm Diameter tube sample CBR Bulk sample for CBR testing E Environmental sample (Glass jar, sealed and chilled on site) ASS Acid Sulfate Soil Sample (Plastic bag, air expelled, chilled) B Bulk Sample				S S F F St S VSt N	/ery Soft Soft Firm Stiff /ery Stiff Hard Friable	25 - 50 50 - 10 100 - 20 Stiff 200 - 40		5 - 50 0 - 100 00 - 200 00 - 400	0 W _p Plastic Limit
<u> </u>	G tra De	anges radational or ansitional stra efinitive or dis rata change	ata ,	Field Tests PID Photoionisation detector reading (ppm) DCP(x-y) Dynamic penetrometer test (test depth interval shown) HP Hand Penetrometer test (UCS kPa)			<u>Density</u>				oose n Dense ense	Density Index <15% Density Index 15 - 35% Density Index 35 - 65% Density Index 65 - 85% Density Index 85 - 100%	



MCCLOY GROUP DEVELOPMENT MANAGEMENT PPXGED

PROJECT: PROPOSED SUBDIVISION - STAGES 5 TO 9 JOB NO: NEW15P-0070A

LOCATION: PITT STREET, TERALBA

LOGGED BY: SJK

TEST PIT NO:

VD

Very Dense

Density Index 85 - 100%

TP112

1 OF 1

DATE: 12-1-16 **EQUIPMENT TYPE:** 22 tonne excavator SURFACE RL: 31.5 m **TEST PIT LENGTH:** 3.0 m WIDTH: 1.5 m DATUM: Assumed Field Test Drilling and Sampling Material description and profile information CLASSIFICATION SYMBOL CONSISTENCY DENSITY MOISTURE CONDITION GRAPHIC LOG Test Type Structure and additional METHOD Result DEPTH MATERIAL DESCRIPTION: Soil type, plasticity/particle observations SAMPLES (m) (m) characteristics, colour, minor components TOPSOIL Clayey SAND - fine to coarse grained, dark brown to grey, fines of low to medium plasticity, trace of fine SC grained gravel, root affected. M Encountered 0.30m Sandy CLAY - medium plasticity, pale brown, fine to RESIDUAL SOIL medium grained sand, some tree roots. 0.40m U50 31.0 0.5 St/ ΗP 200 Š 0.55m CI VSt CBR 0.65m Refusal at eastern end HIGHLY WEATHERED ROCK SANDSTONE - fine to medium grained, pale brown D and pale grey, estimated high strength. Hole Terminated at 0.90 m 30.5 1.0 TEST PIT NEW15P-0070 LOGS - STAGES 5 TO 9.GPJ <-DrawingFile>> 20-03-2018 13:33 10.0.000 Datgel Lab and In Situ Tool 30.0 1.5 29.5 2.0 2.5 29.0 NON-CORED BOREHOLE -LEGEND: Moisture Condition Notes, Samples and Tests Consistency UCS (kPa) 50mm Diameter tube sample Verv Soft U۵ VS <25 D Dry Water CBR Bulk sample for CBR testing S 25 - 50 Moist Soft М Water Level Ε Environmental sample F Firm 50 - 100 W Wet (Date and time shown) (Glass jar, sealed and chilled on site) St Stiff 100 - 200 W, Plastic Limit Water Inflow ASS Acid Sulfate Soil Sample VSt Very Stiff 200 - 400 W_L Liquid Limit ■ Water Outflow (Plastic bag, air expelled, chilled) Н Hard >400 В Bulk Sample Fb Friable Strata Changes Ę Field Tests **Density** Very Loose Density Index <15% Gradational or PID Photoionisation detector reading (ppm) Loose Density Index 15 - 35% transitional strata DCP(x-y) Dynamic penetrometer test (test depth interval shown) MD Medium Dense Density Index 35 - 65% Definitive or distict HP Hand Penetrometer test (UCS kPa) D Density Index 65 - 85% strata change



CLIENT: McCLOY DEVELOPMENT MANAGEMENT

PROJECT: PROPOSED SUBDIVISION - STAGES 6 & 9

LOCATION: FISHERMANS DRIVE, TERALBA

JOB NO: NEW15P-0070A

TEST PIT NO:

LOGGED BY:

PAGE:

TP601

1 OF 1

ΒE

DATE: 24-10-17

TEST PIT LENGTH:			1.5 m WIDTH: 0.5 m DATUI					И:					
	Drill	ing and San					Material description and profile information				Field	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plastici characteristics,colour,minor componer		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additiona observations
ш	Not Encountered	0.25m		-		SM	TOPSOIL: Silty SAND - fine to coarse grai fines of low plasticity, root affected.	ned, grey,	D				TOPSOIL
	Ň	D 0.35m		_	171171		0.25m SANDSTONE - fine to coarse grained, recoanse and pale grey, estimated medium strength	— — — — · I-brown I.					HIGHLY WEATHERED ROCK
		0.00111		-			Hole Terminated at 0.35 m Practical Refusal						
				0.5_									
				_									
				_									
				-									
				1.0_									
				-									
				_									
				_									
				1. <u>5</u>									
				-									
				_									
				-									
				2.0									
				-									
				_									
				-									
	END:			Notes, Sa				Consiste				CS (kPa	
Water Water Level (Date and time shown) Water Inflow Water Outflow				U ₅₀ 50mm Diameter tube sample CBR Bulk sample for CBR testing E Environmental sample (Glass jar, sealed and chilled on site)			or CBR testing al sample	VS Very Soft S Soft F Firm St Stiff			<25 25 - 50 50 - 100 100 - 200		D Dry M Moist W Wet W _p Plastic Limit
				ASS	Acid S (Plasti	ulfate S c bag, a	Soil Sample air expelled, chilled)	VSt V	/ery Stiff Hard		20	00 - 400 400	P
Strata Changes Gradational or transitional strata			ata	B Bulk Sample Field Tests PID Photoionisation detector reading (ppm)			L L			Very Loose Loose		Density Index <15% Density Index 15 - 35%	
		efinitive or dis rata change	stict	DCP(x-y) HP			etrometer test (test depth interval shown) ometer test (UCS kPa)		ME D VD	D	lediun ense ery De	n Dense ense	Density Index 35 - 65% Density Index 65 - 85% Density Index 85 - 100%



CLIENT: McCLOY DEVELOPMENT MANAGEMENT

PROJECT: PROPOSED SUBDIVISION - STAGES 6 & 9

LOCATION: FISHERMANS DRIVE, TERALBA

JOB NO: NEW15P-0070A

TEST PIT NO:

LOGGED BY:

PAGE:

TP602

1 OF 1

ΒE

DATE: 24-10-17

EQUIPMENT TYPE: 2.5 TONNE EXCAVATOR SURFACE RL:

		T LENGTH		1.5 m		IDTH:		ACE RL:					
	Drill	ing and Sam	pling				Material description and profile information				Fiel	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity characteristics,colour,minor component		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additiona observations
ш	Not Encountered	0.20m 0.25m		-		SM	FILL: TREE MULCH FILL: TOPSOIL- Silty SAND - fine to coarse dark grey, fines of low plasticity, with some medium grained sub-angular to sub-rounder root affected.	fine to d gravel,	M	D			FILL - MULCH FILL - TOPSOIL RESIDUAL SOIL 7
		D		1.6			Clayey SAND - fine to coarse grained, oran and pale grey-white, trace fine to medium g sub-angular to sub-rounded gravel. SANDSTONE - fine to coarse grained, pale orange-brown and pale grey-white, estimate medium to high strength. Hole Terminated at 0.27 m Practical Refusal	rained 	D			1 N	POSSIBLE COLLUVIUM HIGHLY WEATHERED ROCK
Wate	— Wat (Dat Wat	er Level e and time sh er Inflow er Outflow	own)	Notes, Sa U ₅₀ CBR E	50mm Bulk s Enviro (Glass Acid S	Diame ample f onmenta s jar, se Sulfate S	ts Iter tube sample for CBR testing al sample aled and chilled on site) Soil Sample air expelled, chilled)	S S F F St S VSt V	ncy /ery Soft Soft Stiff /ery Stiff		25 50 10 20	CS (kPa) 225 5 - 50 0 - 100 00 - 200 00 - 400 400	Moisture Condition D Dry M Moist W Wet W _p Plastic Limit W _L Liquid Limit
Stra	ta Cha G tra De	anges radational or ansitional strat efinitive or dist rata change	ta	B Field Test PID DCP(x-y) HP	Bulk S s Photo Dynar	Sample ionisationis	on detector reading (ppm) etrometer test (test depth interval shown) ometer test (UCS kPa)	I	riable V L MD D VD	Lo M D	ery Lo	oose n Dense	Density Index <15% Density Index 15 - 35% Density Index 35 - 65% Density Index 65 - 85% Density Index 85 - 100%



CLIENT: McCLOY DEVELOPMENT MANAGEMENT

PROJECT: PROPOSED SUBDIVISION - STAGES 6 & 9

LOCATION: FISHERMANS DRIVE, TERALBA

TP903 TEST PIT NO:

PAGE: 1 OF 1

LOGGED BY:

JOB NO: NEW15P-0070A

ΒE

DATE: 24-10-17

EQUIPMENT TYPE: 2.5 TONNE EXCAVATOR SURFACE RL: TEST PIT I ENGTH-15 m WIDTH: 05 m DATI IM:

TES	ST PI	T LENGTI	H:	1.5 m	W	IDTH:	0.5 m DAT	UM:					
	Drill	ing and San					Material description and profile information				Field	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plastic characteristics,colour,minor compone		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations
	red						0.05m FILL: TREE MULCH		М				FILL - MULCH
Е	ot Encountered			_		sc	FILL-TOPSOIL: Clayey SAND - fine to coo grained, dark grey, fines of low to medium with some fine to medium grained sub-an- sub-rounded gravel.	plasticity,	W - M				FILL - TOPSOIL
	Not						SANDSTONE - fine to coarse grained, pa	- — — — <i>—</i> le	D	VD			HIGHLY WEATHERED ROCK
				-			orange-brown and pale grey-white, estimated medium to high strength.	ated /	/				
				_			Hole Terminated at 0.25 m Practical Refusal						
				0.5			Fractical Netusal						
				0.5_									
				-									
				-									
				_									
				1.0									
				-									
				_									
				-									
				1.5									
				-									
				_									
				-									
				2.0									
				-									
LEG Wat													
LEG	END:		<u> </u>	Notes, Sai	_		_	Consiste			_	CS (kPa	•
Wat		er Level		U₅₀ CBR			ter tube sample or CBR testing	s s	/ery Soft Soft	L		25 5 - 50	D Dry M Moist
=		er Levei e and time sl	hown)	E			al sample aled and chilled on site)	1	Firm Stiff			0 - 100 00 - 200	W Wet W₀ Plastic Limit
-		er Inflow	1	ASS	Acid S	Sulfate S	Soil Sample	VSt '	ery Stiff	:	20	00 - 400	P
Stra		er Outflow anges		В	Bulk S	ic bag, : Sample	air expelled, chilled)	1	Hard Friable		>/	400	
	Gi	radational or		Field Test PID	<u>s</u>		on detector reading (ppm)	Density	V L		ery Lo	oose	Density Index <15% Density Index 15 - 35%
ı	tra	ansitional stra		DCP(x-y)			etrometer test (test depth interval shown)					n Dense	
	_ De	efinitive or dis	stict	HP			ometer test (UCS kPa)		ME D		ense	II Delise	Density Index 65 - 85%



CLIENT: McCLOY TERALBA

PROJECT: PROPOSED SUBDIVISION - STAGE 8

LOCATION: FISHERMANS DRIVE, TERALBA

LOGGED BY: ΒE DATE: 13-5-16

TEST PIT NO:

PAGE:

JOB NO:

TP204

1 OF 1

NEW15P - 0070A

FOLIIPMENT TYPE: KORELCO - 5.5 Tonne Excavator SLIDEVCE DI -31 5 m

		IENT TYPI T LENGTI		KOBE 2.0 m		5.5 To I DTH:	onne Excavator 0.3 m	SURFACE DATUM:	RL:		1.5 m Assum			
	Drill	ing and San	npling				Material description and	profile information				Fiel	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL		N: Soil type, plasticity/partic ur,minor components	cle	MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additiona observations
	70			_		SM	Silty SAND - fine to me affected.	dium grained, grey, root		D - M				TOPSOIL
	untere			_	<u> Σ Σ </u> :	 SP	SAND - fine to medium	grained, grey to		D - IVI	MD - D			COLLUVIUM
ш	Not Encountered	0.30m		-		CI	o.27m yellow-brown. Sandy CLAY - medium o.40m orange-brown, fine to r	to high plasticity, orange a	nd	- M - N - N - N - N - N - N - N - N - N	Н	HP	>600	RESIDUAL SOIL
	No	8:48m D	31.0	0.5			SANDSTONE - fine to and white, low plasticity strength.	medium grained, pale oran r, estimated very low to low	/	_ ≥				EXTREMELY TO HIGHLY WEATHERED ROCK
		0.65m		-			Hole Terminated at 0.6 Refusal on weathered							
			30.5	1.0										
				-										
				-										
			30.0	1.5										
			29.5	2.0										
			-											
				_										
			29.0	2.5										
				-										
				-										
LEG Wate	Wat (Dat	er Level e and time sh	nown)	Notes, Sai U ₅₀ CBR E	50mm Bulk s Enviro (Glass	Diame ample f nmenta jar, se	ter tube sample or CBR testing al sample aled and chilled on site) Soil Sample	Con VS S F St VSt	Sol Firr Stif	ry Soft ft m		-25 25 50 10	CS (kPa 25 5 - 50 0 - 100 00 - 200 00 - 400	D Dry M Moist W Wet W _p Plastic Limit
		er Outflow anges		В	(Plasti Bulk S		air expelled, chilled)	H Fb	Ha Fria	rd able		>4	400	
	G tra — D	radational or ansitional stra efinitive or dis rata change	ıta	Field Test PID DCP(x-y) HP	Photoi Dynan	nic pen	on detector reading (ppm) etrometer test (test depth interva emeter test (UCS kPa)	shown)	sity	V L MD D VD	Lo M D	ery Lo oose lediun ense	n Dense	Density Index <15% Density Index 15 - 35% Density Index 35 - 65% Density Index 65 - 85%



CLIENT: McCLOY TERALBA

PROJECT: PROPOSED SUBDIVISION - STAGE 5

LOCATION: FISHERMANS DRIVE, TERALBA

DRIVE, TERALBA LOGGED BY: SJK
DATE: 28-7-17

TEST PIT NO:

PAGE:

JOB NO:

TP5-3

1 OF 1

NEW15P - 0070A

EQUIPMENT TYPE: 5 TONNE EXCAVATOR SURFACE RL:

	Drill	ing and Sam	pling				Material description and profile information				Field	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticit characteristics,colour,minor componen		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additiona observations
				_		sc	0.05m FILL: MULCH - grey to brown. FILL-TOPSOIL: Clayey SAND - fine to coa grained, grey, fines of low to medium plasti	citv. with	М				FILL - MULCH FILL - TOPSOIL
	itered	0.55m		- 0.5_ -		CI	FILL: Sandy CLAY / Gravelly Clayey SANL plasticity, grey to brown, with brown to orar pale grey, fine to coarse grained sand, with fine to coarse grained gravel, trace cobble fragments.	o - medium ge and some	$M \sim W_P$	VSt			CONTROLLED FILL
В	Not Encountered	U50 0.75m		-		CI	FILL: Sitty Gravelly SAND - fine to coarse of pale brown with pale grey to white, fine to of grained gravel, fines of low plasticity, with scobble sized rock fragments.	oarse	М	D			
				1. <u>0</u>		СН	Sandy CLAY - medium to high plasticity, br red, pale grey and orange to brown, fine to grained sand.		M > W _P	VSt	HP	300	RESIDUAL SOIL
				1.5	<i>[[]]</i>		Hole Terminated at 1.50 m						
				2.0									
				-									
				2.5									
				-									
<u>Wat</u>	Wat (Dat Wat Wat	er Level te and time sh er Inflow er Outflow anges	own)	Notes, San U ₅₀ CBR E ASS	50mm Bulk s Enviro (Glass Acid S (Plasti	Diame ample t nmenta jar, se ulfate \$	ts ter tube sample for CBR testing al sample aled and chilled on site) Soil Sample air expelled, chilled)	S S F F St S VSt V H F	ncy Yery Soft Soft Sirm Stiff Yery Stiff Hard Friable		25 50 10 20	CS (kPa 25 5 - 50 0 - 100 00 - 200 00 - 400 400	D Dry M Moist W Wet D W _p Plastic Limit
<u> </u>	G tra D	radational or ansitional strat efinitive or dist rata change		Field Test PID DCP(x-y) HP	<u>s</u> Photoi Dynan	onisatio	on detector reading (ppm) etrometer test (test depth interval shown) ometer test (UCS kPa)	Density	V L ME D VD	Lo D D	ery Lo oose lediun ense	n Dense	Density Index <15% Density Index 15 - 35% e Density Index 35 - 65% Density Index 65 - 85% Density Index 85 - 100%



CLIENT: McCLOY TERALBA

PROJECT: PROPOSED SUBDIVISION - STAGE 5

LOCATION: FISHERMANS DRIVE, TERALBA

DATE: 28-7-17

TEST PIT NO:

LOGGED BY:

PAGE:

JOB NO:

TP5-5

1 OF 1

SJK

NEW15P - 0070A

EQUIPMENT TYPE: CASE BACKHOE 580ST **SURFACE RL**:

			T LENGTH		1.5 m		IDTH:	0.5 m DATU	ACE RL: JM:					
		Drill	ing and Sam	pling				Material description and profile information				Field	d Test	
	METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity characteristics,colour,minor component		MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations
					-		sc	0.05m FILL: MULCH - grey to brown FILL-TOPSOIL: Clayey SAND - fine to coat grained, grey, fines of low to medium plasti some fine to medium grained gravel and or	city, with	M - W				FILL - MULCH FILL - TOPSOIL
ab and in Situ Tool	ВН	Not Encountered	0.40m U50 0.80m		- 0. <u>5</u> - - - 1. <u>0</u>		СН	FILL: Sandy CLAY - medium to high plastic brown to orange, brown to red, pale grey, fi coarse grained sand, some fine to coarse g sub-angular gravel.	ne to	M > W _P	VSt	HP	350	CONTROLLED FILL
10.0.000 Datgel La					-		CH	CLAY - medium to high plasticity, pale brow brown to red and grey, with some fine to me grained sand.	 vn with edium	-	St - VSt	HP	200	RESIDUAL SOIL
QTLIB 1.1.GLB Log NON-CORED BOREHOLE - TEST PIT NEW15P - 0070A LOGS - STAGE 5 FOLLOWING REGRADE.GPJ <-DrawingFile>> 20-03-2018 13:37 10.0.000 Datyel Lab and in Situ Tool		ENIT			1.5			Hole Terminated at 1.40 m						Maintage Occupie
1.GLB Log NON-CORED BOREHOLE	Wate	Wat (Dat Wat Wat ta Cha	er Level e and time sh er Inflow er Outflow anges radational or ansitional stra	own)	Notes, Sa U ₅₀ CBR E ASS B Field Test	50mm Bulk s Enviro (Glass Acid S (Plasti Bulk S	Diame ample fanmenta i jar, se sulfate Sc bag, a ample onisatio	Ter tube sample or CBR testing all sample alled and chilled on site) Soil Sample air expelled, chilled) on detector reading (ppm)	S S F Fi St S VSt V	ery Soft oft irm tiff ery Stiff ard riable V L	Vi Lo	25 50 10 20 20 20 ery Lo	5 - 50 0 - 100 00 - 200 00 - 400 400 pose	D Dry M Moist W Wet W, Plastic Limit W Liquid Limit Density Index <15% Density Index 15 - 35%
QT LIB 1.1			efinitive or dis rata change	tict	DCP(x-y) HP			etrometer test (test depth interval shown) meter test (UCS kPa)		MD D VD	D	ediun ense ery De	n Dense ense	Density Index 35 - 65% Density Index 65 - 85% Density Index 85 - 100%

APPENDIX B:

Results of Laboratory Testing



02 4968 4468 T: 02 4960 9775 E: admin@qualtest.com.au W: www.qualtest.com.au ABN: 98 153 268 896

Report No: MAT: NEW18W-0698--S01

Issue No: 2

is report replaces all previous issues of report no 'MAT:NEW18W-0698--S01'.



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The results of the tests, calibrations and/or measurements included in this document are traceable to Australian/national standards

D. (W)

Approved Signatory: Dane Cullen (Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 16/03/2018

Material Test Report

McCloy Development Management Pty Ltd Suite 1 Level 3, 426 King Street

Newcastle West NSW 2300

Principal:

Project No.: NEW15P-0070A

Project Name: Proposed Subdivision - Billy's Lookout - Stage 7

Sample Details

Sample ID: NEW18W-0698--S01 Sampling Method: AS1289.1.2.1 cl 6.4b

Date Sampled: 06/03/2018 Source: On-Site Material: Silty Clay Specification: No Specification Project Location: Pitt Street, Teralba Sample Location: TP-701 - (0.8 - 1.0m)

Test Results

Description	Method	Result Limits
Sample History	AS 1289.1.1	Air-dried
Preparation	AS 1289.1.1	Dry Sieved
Linear Shrinkage (%)	AS 1289.3.4.1	9.0
Mould Length (mm)		250
Crumbling		No
Curling		No
Cracking		Yes
Liquid Limit (%)	AS 1289.3.1.1	52
Method		Four Point
Plastic Limit (%)	AS 1289.3.2.1	17
Plasticity Index (%)	AS 1289.3.3.1	35

Comments



02 4968 4468 T: 02 4960 9775 E: admin@qualtest.com.au W: www.qualtest.com.au ABN: 98 153 268 896

Report No: MAT:NEW18W-0698--S02

Issue No: 2

is report replaces all previous issues of report no 'MAT:NEW18W-0698--S02'.



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The results of the tests, calibrations and/or measurements included in this document are traceable to Australian/national standards

D. (1)

Approved Signatory: Dane Cullen (Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 16/03/2018

Newcastle West NSW 2300

Principal:

Project No.: NEW15P-0070A

Material Test Report

Project Name: Proposed Subdivision - Billy's Lookout - Stage 7

McCloy Development Management Pty Ltd Suite 1 Level 3, 426 King Street

Sample Details

Sample ID: NEW18W-0698--S02 Sampling Method: AS1289.1.2.1 cl 6.4b

Date Sampled: 06/03/2018 Source: On-Site Material: Clayey Sand Specification: No Specification Project Location: Pitt Street, Teralba Sample Location: TP-702 - (0.4 - 0.6m)

Test Results

Description	Method	Result Limit
Sample History	AS 1289.1.1	Air-dried
Preparation	AS 1289.1.1	Dry Sieved
Linear Shrinkage (%)	AS 1289.3.4.1	7.0
Mould Length (mm)		250
Crumbling		No
Curling		No
Cracking		Yes
Liquid Limit (%)	AS 1289.3.1.1	39
Method		Four Point
Plastic Limit (%)	AS 1289.3.2.1	18
Plasticity Index (%)	AS 1289.3.3.1	21

Comments



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Report No: MAT:NEW18W-0698--S03

Issue No: 2

is report replaces all previous issues of report no 'MAT:NEW18W-0698--S03'.



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D. (1) Approved Signatory: Dane Cullen (Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 16/03/2018

Material Test Report

McCloy Development Management Pty Ltd Suite 1 Level 3, 426 King Street

Newcastle West NSW 2300

Principal:

Project No.: NEW15P-0070A

Project Name: Proposed Subdivision - Billy's Lookout - Stage 7

Sample Details

Sample ID: NEW18W-0698--S03 Sampling Method: AS1289.1.2.1 cl 6.4b

Date Sampled: 06/03/2018 Source: On-Site Material: Sandy Clay Specification: No Specification Project Location: Pitt Street, Teralba Sample Location: TP-703 - (0.05 - 0.2m)

Test Results

Description	Method	Result Limits
Sample History	AS 1289.1.1	Air-dried
Preparation	AS 1289.1.1	Dry Sieved
Linear Shrinkage (%)	AS 1289.3.4.1	3.5
Mould Length (mm)		250
Crumbling		No
Curling		No
Cracking		Yes
Liquid Limit (%)	AS 1289.3.1.1	24
Method		Four Point
Plastic Limit (%)	AS 1289.3.2.1	16
Plasticity Index (%)	AS 1289.3.3.1	8

Comments



Material Test Report

McCloy Development Management Pty Ltd Suite 1 Level 3, 426 King Street

Newcastle West NSW 2300

Project Name: Proposed Subdivision - Billy's Lookout - Stage 7

QUALTEST Laboratory (NSW) Pty Ltd (20708) 8 Ironbark Close Warabrook NSW 2304

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Report No: MAT:NEW18W-0698--S04

Issue No: 2

is report replaces all previous issues of report no 'MAT:NEW18W-0698--S04'.



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The results of the tests, calibrations and/or measurements included in this document are traceable to Australian/national standards

D. (1)

Approved Signatory: Dane Cullen (Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 16/03/2018

WORLD RECOGNISED ACCREDITATION

Sample Details

Principal:

Project No.:

Sample ID: NEW18W-0698--S04 Sampling Method: AS1289.1.2.1 cl 6.4b

NEW15P-0070A

Date Sampled: 06/03/2018 Source: On-Site Material: Clayey Sand Specification: No Specification Project Location: Pitt Street, Teralba Sample Location: TP-704 - (0.2 - 0.4m)

Test Results

Description	Method	Result Limits
Sample History	AS 1289.1.1	Air-dried
Preparation	AS 1289.1.1	Dry Sieved
Linear Shrinkage (%)	AS 1289.3.4.1	4.0
Mould Length (mm)		250
Crumbling		No
Curling		No
Cracking		Yes
Liquid Limit (%)	AS 1289.3.1.1	26
Method		Four Point
Plastic Limit (%)	AS 1289.3.2.1	17
Plasticity Index (%)	AS 1289.3.3.1	9

Comments



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Material Test Report

McCloy Development Management Pty Ltd Suite 1 Level 3, 426 King Street

Newcastle West NSW 2300

Principal:

Project No.: NEW15P-0070A

Project Name: Proposed Subdivision - Billy's Lookout - Stage 7

Report No: MAT:NEW18W-0698--S05

Issue No: 2

is report replaces all previous issues of report no 'MAT:NEW18W-0698--S05'.



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D. (1) Approved Signatory: Dane Cullen (Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 16/03/2018

Sample Details

Sample ID: NEW18W-0698--S05 Sampling Method: AS1289.1.2.1 cl 6.4b

Date Sampled: 06/03/2018 Source: On-Site Material: Sandy Clay Specification: No Specification Project Location: Pitt Street, Teralba Sample Location: TP-705 - (0.1 - 0.2m)

Test Results

Description	Method	Result Limits
Sample History	AS 1289.1.1	Air-dried
Preparation	AS 1289.1.1	Dry Sieved
Linear Shrinkage (%)	AS 1289.3.4.1	3.0
Mould Length (mm)		250
Crumbling		No
Curling		No
Cracking		Yes
Liquid Limit (%)	AS 1289.3.1.1	24
Method		Four Point
Plastic Limit (%)	AS 1289.3.2.1	18
Plasticity Index (%)	AS 1289.3.3.1	6

Comments



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Report No: MAT:NEW18W-0698--S06

Issue No: 2

is report replaces all previous issues of report no 'MAT:NEW18W-0698--S06'.



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The results of the tests, calibrations and/or

measurements included in this document are traceable to Australian/national standards

D. (1) Approved Signatory: Dane Cullen (Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 16/03/2018

WORLD RECOGNISED ACCREDITATION

Principal:

Project No.: NEW15P-0070A

Material Test Report

Project Name: Proposed Subdivision - Billy's Lookout - Stage 7

Newcastle West NSW 2300

McCloy Development Management Pty Ltd Suite 1 Level 3, 426 King Street

Sample Details

Sample ID: NEW18W-0698--S06 Sampling Method: AS1289.1.2.1 cl 6.4b

Date Sampled: 06/03/2018 Source: On-Site Material: Clayey Sand Specification: No Specification Project Location: Pitt Street, Teralba Sample Location: TP-706 - (0.3 - 0.5m)

Test Results

Description	Method	Result Limits
Sample History	AS 1289.1.1	Air-dried
Preparation	AS 1289.1.1	Dry Sieved
Linear Shrinkage (%)	AS 1289.3.4.1	3.5
Mould Length (mm)		250
Crumbling		No
Curling		No
Cracking		Yes
Liquid Limit (%)	AS 1289.3.1.1	27
Method		Four Point
Plastic Limit (%)	AS 1289.3.2.1	17
Plasticity Index (%)	AS 1289.3.3.1	10

Comments



02 4968 4468 T: 02 4960 9775 E: admin@qualtest.com.au W: www.qualtest.com.au ABN: 98 153 268 896

Report No: MAT:NEW18W-0698--S07

Issue No: 1

Material Test Report

McCloy Development Management Pty Ltd Suite 1 Level 3, 426 King Street

Newcastle West NSW 2300

Principal:

Project No.: NEW15P-0070A

Project Name: Proposed Subdivision - Billy's Lookout - Stages 6 & 9



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D. (D)

Approved Signatory: Dane Cullen (Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 14/03/2018

Sample Details

Sample ID: NEW18W-0698--S07 Sampling Method: AS1289.1.2.1 cl 6.4b

Date Sampled: 06/03/2018 Source: On-Site Material: Sandstone Specification: No Specification Project Location: Pitt Street, Teralba Sample Location: TP-707 - (0.6 - 0.7m)

Test Results

Description	Method	Result Limits
Sample History	AS 1289.1.1	Air-dried
Preparation	AS 1289.1.1	Dry Sieved
Linear Shrinkage (%)	AS 1289.3.4.1	5.0
Mould Length (mm)		250
Crumbling		No
Curling		No
Cracking		Yes
Liquid Limit (%)	AS 1289.3.1.1	30
Method		Four Point
Plastic Limit (%)	AS 1289.3.2.1	15
Plasticity Index (%)	AS 1289.3.3.1	15

Comments



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Report No: MAT:NEW18W-0698--S08

Issue No: 2

is report replaces all previous issues of report no 'MAT:NEW18W-0698--S08'.



D. (1)

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Approved Signatory: Dane Cullen (Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 16/03/2018

Material Test Report

McCloy Development Management Pty Ltd Suite 1 Level 3, 426 King Street

Newcastle West NSW 2300

Principal:

Project No.: NEW15P-0070A

Project Name: Proposed Subdivision - Billy's Lookout - Stage 7

Sample Details

Sample ID: NEW18W-0698--S08 Sampling Method: AS1289.1.2.1 cl 6.4b

Date Sampled: 06/03/2018 Source: On-Site Material: Sandstone Specification: No Specification Project Location: Pitt Street, Teralba Sample Location: TP-708 - (0.3 - 0.5m)

Test Results

Description	Method	Result Limits
Sample History	AS 1289.1.1	Air-dried
Preparation	AS 1289.1.1	Dry Sieved
Linear Shrinkage (%)	AS 1289.3.4.1	4.0
Mould Length (mm)		250
Crumbling		No
Curling		No
Cracking		Yes
Liquid Limit (%)	AS 1289.3.1.1	26
Method		Four Point
Plastic Limit (%)	AS 1289.3.2.1	16
Plasticity Index (%)	AS 1289.3.3.1	10

Comments



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Report No: MAT:NEW18W-0698--S09

Issue No: 2

is report replaces all previous issues of report no 'MAT:NEW18W-0698--S09'.



D. (1)

Accredited for compliance with ISO/IEC 17025 -

Testing
The results of the tests, calibrations and/or measurements included in this document are traceable to Australian/national standards

Approved Signatory: Dane Cullen (Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 16/03/2018

Material Test Report

McCloy Development Management Pty Ltd Suite 1 Level 3, 426 King Street

Newcastle West NSW 2300

Principal:

Project No.: NEW15P-0070A

Project Name: Proposed Subdivision - Billy's Lookout - Stage 7

Sample Details

Sample ID: NEW18W-0698--S09 Sampling Method: AS1289.1.2.1 cl 6.4b

Date Sampled: 06/03/2018 Source: On-Site Material: Clayey Sand Specification: No Specification Project Location: Pitt Street, Teralba Sample Location: TP-711 - (0.1 - 0.2m)

Test Results

Description	Method	Result Limits
Sample History	AS 1289.1.1	Air-dried
Preparation	AS 1289.1.1	Dry Sieved
Linear Shrinkage (%)	AS 1289.3.4.1	3.0
Mould Length (mm)		250
Crumbling		No
Curling		No
Cracking		Yes
Liquid Limit (%)	AS 1289.3.1.1	26
Method		Four Point
Plastic Limit (%)	AS 1289.3.2.1	19
Plasticity Index (%)	AS 1289.3.3.1	7

Comments



02 4968 4468 T: 02 4960 9775 E: admin@qualtest.com.au W: www.qualtest.com.au ABN: 98 153 268 896

Report No: MAT:NEW18W-0698--S10

Issue No: 2

is report replaces all previous issues of report no 'MAT:NEW18W-0698--S10'.



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D. (1) Approved Signatory: Dane Cullen (Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 16/03/2018

WORLD RECOGNISED ACCREDITATION

Principal:

Project No.: NEW15P-0070A

Material Test Report

Project Name: Proposed Subdivision - Billy's Lookout - Stage 7

Newcastle West NSW 2300

McCloy Development Management Pty Ltd Suite 1 Level 3, 426 King Street

Sample Details

Sample ID: NEW18W-0698--S10 Sampling Method: AS1289.1.2.1 cl 6.4b

Date Sampled: 06/03/2018 Source: On-Site Material: Sandy Siltstone Specification: No Specification Project Location: Pitt Street, Teralba Sample Location: TP711 - (0.4 - 0.6m)

Test Results

Description	Method	Result Limits
Sample History	AS 1289.1.1	Air-dried
Preparation	AS 1289.1.1	Dry Sieved
Linear Shrinkage (%)	AS 1289.3.4.1	7.0
Mould Length (mm)		250
Crumbling		No
Curling		No
Cracking		Yes
Liquid Limit (%)	AS 1289.3.1.1	36
Method		Four Point
Plastic Limit (%)	AS 1289.3.2.1	16
Plasticity Index (%)	AS 1289.3.3.1	20

Comments



02 4968 4468 T: 02 4960 9775 E: admin@qualtest.com.au W: www.qualtest.com.au ABN: 98 153 268 896

Report No: MAT:NEW18W-0698--S11

Issue No: 2

is report replaces all previous issues of report no 'MAT:NEW18W-0698--S11'.



Accredited for compliance with ISO/IEC 17025 -

Testing
The results of the tests, calibrations and/or measurements included in this document are traceable to Australian/national standards

D. (1) Approved Signatory: Dane Cullen (Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 16/03/2018

Material Test Report

McCloy Development Management Pty Ltd Suite 1 Level 3, 426 King Street

Newcastle West NSW 2300

Principal:

Project No.: NEW15P-0070A

Project Name: Proposed Subdivision - Billy's Lookout - Stage 7

Sample Details

Sample ID: NEW18W-0698--S11 Sampling Method: AS1289.1.2.1 cl 6.4b

Date Sampled: 06/03/2018 Source: On-Site Material: Sandy Clay Specification: No Specification Pitt Street, Teralba Project Location: Sample Location: TP712 - (0.3 - 0.5m)

Test Results

Description	Method	Result Limits
Sample History	AS 1289.1.1	Air-dried
Preparation	AS 1289.1.1	Dry Sieved
Linear Shrinkage (%)	AS 1289.3.4.1	9.0
Mould Length (mm)		250
Crumbling		No
Curling		No
Cracking		Yes
Liquid Limit (%)	AS 1289.3.1.1	52
Method		Four Point
Plastic Limit (%)	AS 1289.3.2.1	21
Plasticity Index (%)	AS 1289.3.3.1	31

Comments



02 4968 4468 T: 02 4960 9775 E: admin@qualtest.com.au W: www.qualtest.com.au ABN: 98 153 268 896

Report No: MAT:NEW18W-0698--S12

Issue No: 2

is report replaces all previous issues of report no 'MAT:NEW18W-0698--S12'.



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The results of the tests, calibrations and/or measurements included in this document are traceable to Australian/national standards

D. (1)

Approved Signatory: Dane Cullen (Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 16/03/2018

Principal:

Project No.: NEW15P-0070A

Material Test Report

Project Name: Proposed Subdivision - Billy's Lookout - Stage 7

Newcastle West NSW 2300

McCloy Development Management Pty Ltd Suite 1 Level 3, 426 King Street

Sample Details

Sample ID: NEW18W-0698--S12 Sampling Method: AS1289.1.2.1 cl 6.4b

Date Sampled: 06/03/2018 Source: On-Site Material: Sandy Siltstone Specification: No Specification Project Location: Pitt Street, Teralba Sample Location: TP714 - (0.3 - 0.5m)

Test Results

Description	Method	Result Limits
Sample History	AS 1289.1.1	Air-dried
Preparation	AS 1289.1.1	Dry Sieved
Linear Shrinkage (%)	AS 1289.3.4.1	7.0
Mould Length (mm)		250
Crumbling		No
Curling		No
Cracking		Yes
Liquid Limit (%)	AS 1289.3.1.1	43
Method		Four Point
Plastic Limit (%)	AS 1289.3.2.1	20
Plasticity Index (%)	AS 1289.3.3.1	23

Comments



Material Test Report

McCloy Teralba Pty Ltd

Suite 1, Level 3, 426 King Street Newcastle West NSW 2300

Project Name: Proposed Subdivision - Billy's Lookout - Stage 5 to 9

QUALTEST Laboratory (NSW) Pty Ltd (20708) 8 Ironbark Close Warabrook NSW 2304

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Report No: MAT:NEW16W-1263--S11

Issue No: 2

is report replaces all previous issues of report no 'MAT:NEW16W-1263--S11'.



Accredited for compliance with ISO/IEC 17025
The results of the tests, calibrations and/or measurements included in this document are traceable to Australian/national standards

Approved Signatory: Dane Cullen (Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 8/06/2016

WORLD RECOGNISED ACCREDITATION

Sample Details

Client:

Principal: Project No.:

Sample ID: NEW16W-1263--S11 Sampling Method: AS1289.1.2.1 cl 6.5

NEW15P-0070A

Date Sampled: 13/05/2016 Source: On-Site Material: Sandy Clay Specification: No Specification Pitt Street, Teralba Project Location: Sample Location: TP204 - (0.3 - 0.4m)|

Test Results

Description	Method	Result Limits
Sample History	AS 1289.1.1	Air-dried
Preparation	AS 1289.1.1	Dry Sieved
Linear Shrinkage (%)	AS 1289.3.4.1	16.0
Mould Length (mm)		250
Crumbling		No
Curling		No
Cracking		No
Liquid Limit (%)	AS 1289.3.1.1	68
Method		Four Point
Plastic Limit (%)	AS 1289.3.2.1	19
Plasticity Index (%)	AS 1289.3.3.1	49

Comments



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Report No: MAT: NEW17W-4926--S01

Issue No: 1

Material Test Report

McCloy Development Management Pty Ltd Suite 1 Level 3, 426 King Street

Newcastle West NSW 2300

Principal:

Project No.: NEW15P-0070A

Project Name: Proposed Subdivision - Billy's Lookout - Stages 6 & 9



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D. (D)

Approved Signatory: Dane Cullen (Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 9/11/2017

Sample Details

Sample ID: NEW17W-4926--S01 Sampling Method: AS1289.1.2.1 cl 6.4b

Date Sampled: 24/10/2017 Source: On-Site Material: Sandy Clay Specification: No Specification Pitt Street, Teralba Project Location: Sample Location: TP602 - (0.2 - 0.25m)

Test Results

Description	Method	Result Limits
Sample History	AS 1289.1.1	Air-dried
Preparation	AS 1289.1.1	Dry Sieved
Linear Shrinkage (%)	AS 1289.3.4.1	3.5
Mould Length (mm)		250
Crumbling		No
Curling		No
Cracking		Yes
Liquid Limit (%)	AS 1289.3.1.1	27
Method		Four Point
Plastic Limit (%)	AS 1289.3.2.1	17
Plasticity Index (%)	AS 1289.3.3.1	10

Comments



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Report No: MAT: NEW17W-4926--S05

Issue No: 1

Material Test Report

McCloy Development Management Pty Ltd Suite 1 Level 3, 426 King Street

Newcastle West NSW 2300

Principal:

Project No.: NEW15P-0070A

Project Name: Proposed Subdivision - Billy's Lookout - Stages 6 & 9



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Testing
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measurements included in this document are traceable to Australian/national standards

D. (D)

Approved Signatory: Dane Cullen (Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 6/11/2017

Sample Details

Sample ID: NEW17W-4926--S05 Sampling Method: AS1289.1.2.1 cl 6.4b

Date Sampled: 24/10/2017 Source: On-Site Material: Clayey Sand Specification: No Specification Pitt Street, Teralba Project Location: Sample Location: TP903 - (0.1 - 0.2m)

Test Results

Description	Method	Result Limits
Sample History	AS 1289.1.1	Air-dried
Preparation	AS 1289.1.1	Dry Sieved
Linear Shrinkage (%)	AS 1289.3.4.1	3.0
Mould Length (mm)		250
Crumbling		No
Curling		No
Cracking		Yes
Liquid Limit (%)	AS 1289.3.1.1	23
Method		Four Point
Plastic Limit (%)	AS 1289.3.2.1	15
Plasticity Index (%)	AS 1289.3.3.1	8

Comments



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Shrink Swell Index Report

McCloy Development Management Pty Ltd

Suite 1 Level 3, 426 King Street Newcastle West NSW 2300

Principal:

Project No.: NEW15P-0070A

Project Name: Proposed Subdivision - Billy's Lookout - Stage 5

Report No: SSI:NEW17W-3159--S05

Issue No: 2

his report replaces all previous issues of report no 'SSI:NEW17W-3159--S05'



Accredited for compliance with ISO/IEC 17025 -Testing
The results of the tests, calibrations and/or

measurements included in this document are traceable to Australian/national standards

Approved Signatory: Dane Cullen

(Senior Geotechnician)

NATA Accredited Laboratory Number: 18686 Date of Issue: 11/08/2017

Sample Details

Sample ID: NEW17W-3159--S05

Test Request No.:

Material: Sandy Clay Source: On-Site No Specification Specification:

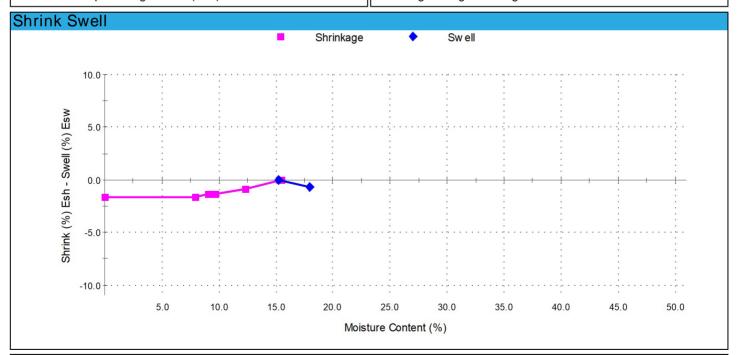
Project Location: Pitt Street, Teralba TP5-5 - (0.4 - 0.8m) Sample Location:

Borehole Number: TP5-5 Borehole Depth (m): 0.4 - 0.8 Client Sample ID:

Sampling Method: AS1289.1.2.1 cl 6.5.4

Date Sampled: 28/07/2017 Date Submitted: 31/07/2017

Swell Test	AS 1289.7.1.1	Shrink Test		AS 1289.7.1	1.1
Swell on Saturation (%):	-0.7	Shrink on drying (%):	1.6		
Moisture Content before (%):	15.2	Shrinkage Moisture Content (%):	15.4		
Moisture Content after (%):	17.9	Est. inert material (%):	15%		
Est. Unc. Comp. Strength before (kPa):	>600	Crumbling during shrinkage:	Nil		
Est. Unc. Comp. Strength after (kPa):	550	Cracking during shrinkage:	Minor		



Shrink Swell Index - Iss (%): 0.9

Comments



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Shrink Swell Index Report

McCloy Teralba Pty Ltd

Suite 1, Level 3, 426 King Street Newcastle West NSW 2300

Principal:

NEW15P-0070A Project No.:

Project Name: Proposed Subdivision - Billy's Lookout - Stage 5 to 9

Report No: SSI:NEW16W-0030--S01 Issue No: 1



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Approved Signatory: Dane Cullen

(Senior Geotechnician) NATA Accredited Laboratory Number: 18686 Date of Issue: 22/01/2016

Sample Details

Sample ID: NEW16W-0030--S01

Test Request No.: Material: CLAY Source: On-Site

Specification: No Specification Project Location: Pitt Street, Teralba TP105 - 0.4 to 0.8m Sample Location:

Borehole Number: Borehole Depth (m): 0.4 to 0.8m Client Sample ID: Sampling Method:

AS1289.1.2.1 cl 6.5

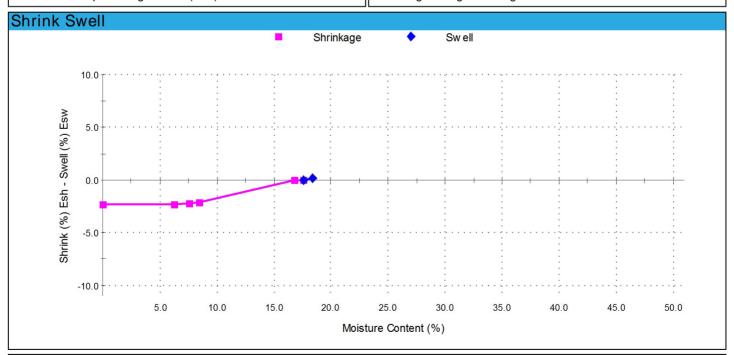
Date Sampled: 12/01/2016 Date Submitted: 14/01/2015

AS 1289.7.1.1 Swell Test

Swell on Saturation (%): 0.2 Moisture Content before (%): 17.6 Moisture Content after (%): 18.4 Est. Unc. Comp. Strength before (kPa): 500 Est. Unc. Comp. Strength after (kPa):

AS 1289.7.1.1 Shrink Test

Shrink on drying (%): 2.3 Shrinkage Moisture Content (%): 17.6 Est. inert material (%): Nil Crumbling during shrinkage: Cracking during shrinkage: Moderate



Shrink Swell Index - Iss (%): 1.3

Comments



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Shrink Swell Index Report

McCloy Teralba Pty Ltd

Suite 1, Level 3, 426 King Street Newcastle West NSW 2300

Principal:

NEW15P-0070A Project No.:

Project Name: Proposed Subdivision - Billy's Lookout - Stage 5 to 9

Report No: SSI:NEW16W-0030--S03 Issue No: 1



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Approved Signatory: Dane Cullen

(Senior Geotechnician) NATA Accredited Laboratory Number: 18686 Date of Issue: 22/01/2016

Sample Details

Sample ID: NEW16W-0030--S03

Test Request No.:

Material: Sandy CLAY Source: On-Site Specification: No Specification

Project Location: Pitt Street, Teralba TP112 - 0.3 to 0.55m Sample Location:

Borehole Number: Borehole Depth (m): 0.3 to 0.55m Client Sample ID: Sampling Method:

AS1289.1.2.1 cl 6.5

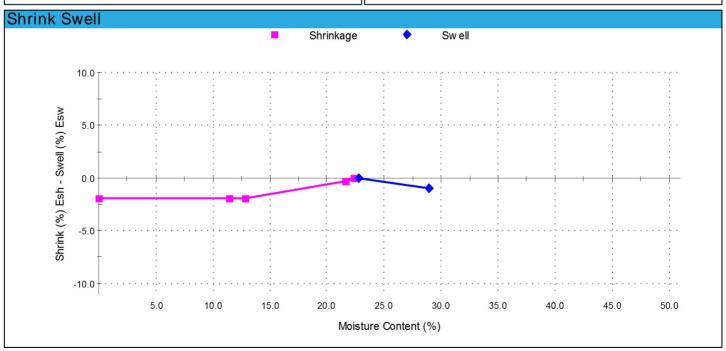
Date Sampled: 12/01/2016 Date Submitted: 14/01/2015

AS 1289.7.1.1 Swell Test

Swell on Saturation (%): -1.0 22.8 Moisture Content before (%): Moisture Content after (%): 29.0 Est. Unc. Comp. Strength before (kPa): 180 Est. Unc. Comp. Strength after (kPa):

AS 1289.7.1.1 Shrink Test

Shrink on drying (%): 1.9 Shrinkage Moisture Content (%): 22.4 Est. inert material (%): Nil Crumbling during shrinkage: Cracking during shrinkage: Minor



Shrink Swell Index - Iss (%): 1.1

Comments

APPENDIX C:

CSIRO Sheet BTF 18

Foundation Maintenance and Footing Performance: A Homeowner's Guide

Foundation Maintenance and Footing Performance: A Homeowner's Guide



BTF 18 replaces Information Sheet 10/91

Buildings can and often do move. This movement can be up, down, lateral or rotational. The fundamental cause of movement in buildings can usually be related to one or more problems in the foundation soil. It is important for the homeowner to identify the soil type in order to ascertain the measures that should be put in place in order to ensure that problems in the foundation soil can be prevented, thus protecting against building movement.

This Building Technology File is designed to identify causes of soil-related building movement, and to suggest methods of prevention of resultant cracking in buildings.

Soil Types

The types of soils usually present under the topsoil in land zoned for residential buildings can be split into two approximate groups – granular and clay. Quite often, foundation soil is a mixture of both types. The general problems associated with soils having granular content are usually caused by erosion. Clay soils are subject to saturation and swell/shrink problems.

Classifications for a given area can generally be obtained by application to the local authority, but these are sometimes unreliable and if there is doubt, a geotechnical report should be commissioned. As most buildings suffering movement problems are founded on clay soils, there is an emphasis on classification of soils according to the amount of swell and shrinkage they experience with variations of water content. The table below is Table 2.1 from AS 2870, the Residential Slab and Footing Code.

Causes of Movement

Settlement due to construction

There are two types of settlement that occur as a result of construction:

- Immediate settlement occurs when a building is first placed on its foundation soil, as a result of compaction of the soil under the weight of the structure. The cohesive quality of clay soil mitigates against this, but granular (particularly sandy) soil is susceptible.
- Consolidation settlement is a feature of clay soil and may take
 place because of the expulsion of moisture from the soil or because
 of the soil's lack of resistance to local compressive or shear stresses.
 This will usually take place during the first few months after
 construction, but has been known to take many years in
 exceptional cases.

These problems are the province of the builder and should be taken into consideration as part of the preparation of the site for construction. Building Technology File 19 (BTF 19) deals with these problems.

Erosion

All soils are prone to erosion, but sandy soil is particularly susceptible to being washed away. Even clay with a sand component of say 10% or more can suffer from erosion.

Saturation

This is particularly a problem in clay soils. Saturation creates a bog-like suspension of the soil that causes it to lose virtually all of its bearing capacity. To a lesser degree, sand is affected by saturation because saturated sand may undergo a reduction in volume – particularly imported sand fill for bedding and blinding layers. However, this usually occurs as immediate settlement and should normally be the province of the builder.

Seasonal swelling and shrinkage of soil

All clays react to the presence of water by slowly absorbing it, making the soil increase in volume (see table below). The degree of increase varies considerably between different clays, as does the degree of decrease during the subsequent drying out caused by fair weather periods. Because of the low absorption and expulsion rate, this phenomenon will not usually be noticeable unless there are prolonged rainy or dry periods, usually of weeks or months, depending on the land and soil characteristics.

The swelling of soil creates an upward force on the footings of the building, and shrinkage creates subsidence that takes away the support needed by the footing to retain equilibrium.

Shear failure

This phenomenon occurs when the foundation soil does not have sufficient strength to support the weight of the footing. There are two major post-construction causes:

- · Significant load increase.
- Reduction of lateral support of the soil under the footing due to erosion or excavation.
- In clay soil, shear failure can be caused by saturation of the soil adjacent to or under the footing.

	GENERAL DEFINITIONS OF SITE CLASSES		
Class	Foundation		
A	Most sand and rock sites with little or no ground movement from moisture changes		
S	Slightly reactive clay sites with only slight ground movement from moisture changes		
M	Moderately reactive clay or silt sites, which can experience moderate ground movement from moisture changes		
Н	Highly reactive clay sites, which can experience high ground movement from moisture changes		
Е	Extremely reactive sites, which can experience extreme ground movement from moisture changes		
A to P	Filled sites		
P	Sites which include soft soils, such as soft clay or silt or loose sands; landslip; mine subsidence; collapsing soils; soils subject to erosion; reactive sites subject to abnormal moisture conditions or sites which cannot be classified otherwise		

Tree root growth

Trees and shrubs that are allowed to grow in the vicinity of footings can cause foundation soil movement in two ways:

- Roots that grow under footings may increase in cross-sectional size, exerting upward pressure on footings.
- Roots in the vicinity of footings will absorb much of the moisture in the foundation soil, causing shrinkage or subsidence.

Unevenness of Movement

The types of ground movement described above usually occur unevenly throughout the building's foundation soil. Settlement due to construction tends to be uneven because of:

- Differing compaction of foundation soil prior to construction.
- Differing moisture content of foundation soil prior to construction.

Movement due to non-construction causes is usually more uneven still. Erosion can undermine a footing that traverses the flow or can create the conditions for shear failure by eroding soil adjacent to a footing that runs in the same direction as the flow.

Saturation of clay foundation soil may occur where subfloor walls create a dam that makes water pond. It can also occur wherever there is a source of water near footings in clay soil. This leads to a severe reduction in the strength of the soil which may create local shear failure.

Seasonal swelling and shrinkage of clay soil affects the perimeter of the building first, then gradually spreads to the interior. The swelling process will usually begin at the uphill extreme of the building, or on the weather side where the land is flat. Swelling gradually reaches the interior soil as absorption continues. Shrinkage usually begins where the sun's heat is greatest.

Effects of Uneven Soil Movement on Structures

Erosion and saturation

Erosion removes the support from under footings, tending to create subsidence of the part of the structure under which it occurs. Brickwork walls will resist the stress created by this removal of support by bridging the gap or cantilevering until the bricks or the mortar bedding fail. Older masonry has little resistance. Evidence of failure varies according to circumstances and symptoms may include:

- Step cracking in the mortar beds in the body of the wall or above/below openings such as doors or windows.
- Vertical cracking in the bricks (usually but not necessarily in line with the vertical beds or perpends).

Isolated piers affected by erosion or saturation of foundations will eventually lose contact with the bearers they support and may tilt or fall over. The floors that have lost this support will become bouncy, sometimes rattling ornaments etc.

Seasonal swelling/shrinkage in clay

Swelling foundation soil due to rainy periods first lifts the most exposed extremities of the footing system, then the remainder of the perimeter footings while gradually permeating inside the building footprint to lift internal footings. This swelling first tends to create a dish effect, because the external footings are pushed higher than the internal ones.

The first noticeable symptom may be that the floor appears slightly dished. This is often accompanied by some doors binding on the floor or the door head, together with some cracking of cornice mitres. In buildings with timber flooring supported by bearers and joists, the floor can be bouncy. Externally there may be visible dishing of the hip or ridge lines.

As the moisture absorption process completes its journey to the innermost areas of the building, the internal footings will rise. If the spread of moisture is roughly even, it may be that the symptoms will temporarily disappear, but it is more likely that swelling will be uneven, creating a difference rather than a disappearance in symptoms. In buildings with timber flooring supported by bearers and joists, the isolated piers will rise more easily than the strip footings or piers under walls, creating noticeable doming of flooring.



As the weather pattern changes and the soil begins to dry out, the external footings will be first affected, beginning with the locations where the sun's effect is strongest. This has the effect of lowering the external footings. The doming is accentuated and cracking reduces or disappears where it occurred because of dishing, but other cracks open up. The roof lines may become convex.

Doming and dishing are also affected by weather in other ways. In areas where warm, wet summers and cooler dry winters prevail, water migration tends to be toward the interior and doming will be accentuated, whereas where summers are dry and winters are cold and wet, migration tends to be toward the exterior and the underlying propensity is toward dishing.

Movement caused by tree roots

In general, growing roots will exert an upward pressure on footings, whereas soil subject to drying because of tree or shrub roots will tend to remove support from under footings by inducing shrinkage.

Complications caused by the structure itself

Most forces that the soil causes to be exerted on structures are vertical – i.e. either up or down. However, because these forces are seldom spread evenly around the footings, and because the building resists uneven movement because of its rigidity, forces are exerted from one part of the building to another. The net result of all these forces is usually rotational. This resultant force often complicates the diagnosis because the visible symptoms do not simply reflect the original cause. A common symptom is binding of doors on the vertical member of the frame.

Effects on full masonry structures

Brickwork will resist cracking where it can. It will attempt to span areas that lose support because of subsided foundations or raised points. It is therefore usual to see cracking at weak points, such as openings for windows or doors.

In the event of construction settlement, cracking will usually remain unchanged after the process of settlement has ceased.

With local shear or erosion, cracking will usually continue to develop until the original cause has been remedied, or until the subsidence has completely neutralised the affected portion of footing and the structure has stabilised on other footings that remain effective.

In the case of swell/shrink effects, the brickwork will in some cases return to its original position after completion of a cycle, however it is more likely that the rotational effect will not be exactly reversed, and it is also usual that brickwork will settle in its new position and will resist the forces trying to return it to its original position. This means that in a case where swelling takes place after construction and cracking occurs, the cracking is likely to at least partly remain after the shrink segment of the cycle is complete. Thus, each time the cycle is repeated, the likelihood is that the cracking will become wider until the sections of brickwork become virtually independent.

With repeated cycles, once the cracking is established, if there is no other complication, it is normal for the incidence of cracking to stabilise, as the building has the articulation it needs to cope with the problem. This is by no means always the case, however, and monitoring of cracks in walls and floors should always be treated seriously.

Upheaval caused by growth of tree roots under footings is not a simple vertical shear stress. There is a tendency for the root to also exert lateral forces that attempt to separate sections of brickwork after initial cracking has occurred.

The normal structural arrangement is that the inner leaf of brickwork in the external walls and at least some of the internal walls (depending on the roof type) comprise the load-bearing structure on which any upper floors, ceilings and the roof are supported. In these cases, it is internally visible cracking that should be the main focus of attention, however there are a few examples of dwellings whose external leaf of masonry plays some supporting role, so this should be checked if there is any doubt. In any case, externally visible cracking is important as a guide to stresses on the structure generally, and it should also be remembered that the external walls must be capable of supporting themselves.

Effects on framed structures

Timber or steel framed buildings are less likely to exhibit cracking due to swell/shrink than masonry buildings because of their flexibility. Also, the doming/dishing effects tend to be lower because of the lighter weight of walls. The main risks to framed buildings are encountered because of the isolated pier footings used under walls. Where erosion or saturation cause a footing to fall away, this can double the span which a wall must bridge. This additional stress can create cracking in wall linings, particularly where there is a weak point in the structure caused by a door or window opening. It is, however, unlikely that framed structures will be so stressed as to suffer serious damage without first exhibiting some or all of the above symptoms for a considerable period. The same warning period should apply in the case of upheaval. It should be noted, however, that where framed buildings are supported by strip footings there is only one leaf of brickwork and therefore the externally visible walls are the supporting structure for the building. In this case, the subfloor masonry walls can be expected to behave as full brickwork walls.

Effects on brick veneer structures

Because the load-bearing structure of a brick veneer building is the frame that makes up the interior leaf of the external walls plus perhaps the internal walls, depending on the type of roof, the building can be expected to behave as a framed structure, except that the external masonry will behave in a similar way to the external leaf of a full masonry structure.

Water Service and Drainage

Where a water service pipe, a sewer or stormwater drainage pipe is in the vicinity of a building, a water leak can cause erosion, swelling or saturation of susceptible soil. Even a minuscule leak can be enough to saturate a clay foundation. A leaking tap near a building can have the same effect. In addition, trenches containing pipes can become watercourses even though backfilled, particularly where broken rubble is used as fill. Water that runs along these trenches can be responsible for serious erosion, interstrata seepage into subfloor areas and saturation.

Pipe leakage and trench water flows also encourage tree and shrub roots to the source of water, complicating and exacerbating the problem.

Poor roof plumbing can result in large volumes of rainwater being concentrated in a small area of soil:

 Incorrect falls in roof guttering may result in overflows, as may gutters blocked with leaves etc.

- Corroded guttering or downpipes can spill water to ground.
- Downpipes not positively connected to a proper stormwater collection system will direct a concentration of water to soil that is directly adjacent to footings, sometimes causing large-scale problems such as erosion, saturation and migration of water under the building.

Seriousness of Cracking

In general, most cracking found in masonry walls is a cosmetic nuisance only and can be kept in repair or even ignored. The table below is a reproduction of Table C1 of AS 2870.

AS 2870 also publishes figures relating to cracking in concrete floors, however because wall cracking will usually reach the critical point significantly earlier than cracking in slabs, this table is not reproduced here.

Prevention/Cure

Plumbing

Where building movement is caused by water service, roof plumbing, sewer or stormwater failure, the remedy is to repair the problem. It is prudent, however, to consider also rerouting pipes away from the building where possible, and relocating taps to positions where any leakage will not direct water to the building vicinity. Even where gully traps are present, there is sometimes sufficient spill to create erosion or saturation, particularly in modern installations using smaller diameter PVC fixtures. Indeed, some gully traps are not situated directly under the taps that are installed to charge them, with the result that water from the tap may enter the backfilled trench that houses the sewer piping. If the trench has been poorly backfilled, the water will either pond or flow along the bottom of the trench. As these trenches usually run alongside the footings and can be at a similar depth, it is not hard to see how any water that is thus directed into a trench can easily affect the foundation's ability to support footings or even gain entry to the subfloor area.

Ground drainage

In all soils there is the capacity for water to travel on the surface and below it. Surface water flows can be established by inspection during and after heavy or prolonged rain. If necessary, a grated drain system connected to the stormwater collection system is usually an easy solution.

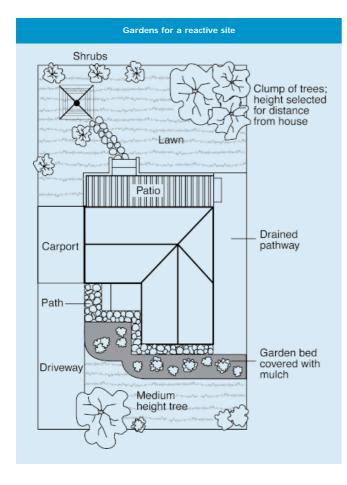
It is, however, sometimes necessary when attempting to prevent water migration that testing be carried out to establish watertable height and subsoil water flows. This subject is referred to in BTF 19 and may properly be regarded as an area for an expert consultant.

Protection of the building perimeter

It is essential to remember that the soil that affects footings extends well beyond the actual building line. Watering of garden plants, shrubs and trees causes some of the most serious water problems.

For this reason, particularly where problems exist or are likely to occur, it is recommended that an apron of paving be installed around as much of the building perimeter as necessary. This paving

CLASSIFICATION OF DAMAGE WITH REFERENCE TO WALLS Description of typical damage and required repair Approximate crack width **Damage** limit (see Note 3) category Hairline cracks < 0.1 mm 0 Fine cracks which do not need repair 1 <1 mm 2 Cracks noticeable but easily filled. Doors and windows stick slightly <5 mm 3 Cracks can be repaired and possibly a small amount of wall will need 5-15 mm (or a number of cracks to be replaced. Doors and windows stick. Service pipes can fracture. 3 mm or more in one group) Weathertightness often impaired Extensive repair work involving breaking-out and replacing sections of walls, 15-25 mm but also depend 4 especially over doors and windows. Window and door frames distort. Walls lean on number of cracks or bulge noticeably, some loss of bearing in beams. Service pipes disrupted



should extend outwards a minimum of 900 mm (more in highly reactive soil) and should have a minimum fall away from the building of 1:60. The finished paving should be no less than 100 mm below brick vent bases.

It is prudent to relocate drainage pipes away from this paving, if possible, to avoid complications from future leakage. If this is not practical, earthenware pipes should be replaced by PVC and backfilling should be of the same soil type as the surrounding soil and compacted to the same density.

Except in areas where freezing of water is an issue, it is wise to remove taps in the building area and relocate them well away from the building – preferably not uphill from it (see BTF 19).

It may be desirable to install a grated drain at the outside edge of the paving on the uphill side of the building. If subsoil drainage is needed this can be installed under the surface drain.

Condensation

In buildings with a subfloor void such as where bearers and joists support flooring, insufficient ventilation creates ideal conditions for condensation, particularly where there is little clearance between the floor and the ground. Condensation adds to the moisture already present in the subfloor and significantly slows the process of drying out. Installation of an adequate subfloor ventilation system, either natural or mechanical, is desirable.

Warning: Although this Building Technology File deals with cracking in buildings, it should be said that subfloor moisture can result in the development of other problems, notably:

- Water that is transmitted into masonry, metal or timber building elements causes damage and/or decay to those elements.
- High subfloor humidity and moisture content create an ideal environment for various pests, including termites and spiders.
- Where high moisture levels are transmitted to the flooring and walls, an increase in the dust mite count can ensue within the living areas. Dust mites, as well as dampness in general, can be a health hazard to inhabitants, particularly those who are abnormally susceptible to respiratory ailments.

The garden

The ideal vegetation layout is to have lawn or plants that require only light watering immediately adjacent to the drainage or paving edge, then more demanding plants, shrubs and trees spread out in that order

Overwatering due to misuse of automatic watering systems is a common cause of saturation and water migration under footings. If it is necessary to use these systems, it is important to remove garden beds to a completely safe distance from buildings.

Existing trees

Where a tree is causing a problem of soil drying or there is the existence or threat of upheaval of footings, if the offending roots are subsidiary and their removal will not significantly damage the tree, they should be severed and a concrete or metal barrier placed vertically in the soil to prevent future root growth in the direction of the building. If it is not possible to remove the relevant roots without damage to the tree, an application to remove the tree should be made to the local authority. A prudent plan is to transplant likely offenders before they become a problem.

Information on trees, plants and shrubs

State departments overseeing agriculture can give information regarding root patterns, volume of water needed and safe distance from buildings of most species. Botanic gardens are also sources of information. For information on plant roots and drains, see Building Technology File 17.

Excavation

Excavation around footings must be properly engineered. Soil supporting footings can only be safely excavated at an angle that allows the soil under the footing to remain stable. This angle is called the angle of repose (or friction) and varies significantly between soil types and conditions. Removal of soil within the angle of repose will cause subsidence.

Remediation

Where erosion has occurred that has washed away soil adjacent to footings, soil of the same classification should be introduced and compacted to the same density. Where footings have been undermined, augmentation or other specialist work may be required. Remediation of footings and foundations is generally the realm of a specialist consultant.

Where isolated footings rise and fall because of swell/shrink effect, the homeowner may be tempted to alleviate floor bounce by filling the gap that has appeared between the bearer and the pier with blocking. The danger here is that when the next swell segment of the cycle occurs, the extra blocking will push the floor up into an accentuated dome and may also cause local shear failure in the soil. If it is necessary to use blocking, it should be by a pair of fine wedges and monitoring should be carried out fortnightly.

This BTF was prepared by John Lewer FAIB, MIAMA, Partner, Construction Diagnosis.

The information in this and other issues in the series was derived from various sources and was believed to be correct when published.

The information is advisory. It is provided in good faith and not claimed to be an exhaustive treatment of the relevant subject.

Further professional advice needs to be obtained before taking any action based on the information provided.

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